## SYSTEMATIC NAVIGATION

## EXCEL APPLICATION FOR ASTRO NAVIGATION

## USER MANUAL V7.0 1-JANUARY-2021

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## 1 Introduction

Systematic Navigation is a Windows and Excel-based solution for astro and offshore navigation.
The object of this manual is to help you get the most out of the application. This manual provides background on the use of Systematic Navigation and the methods used in its formulation. It also provides in a convenient form all the data you need for astronomical navigation and sight planning.

Systematic Navigation solves all the problems of calculating hour angles declination and sight reduction and then plots sight lines and statistical fixes for up to three sights. It is totally automated and removes the need for a pocket calculator, almanac or sight tables and provides:

- Position fixes from two or three sextant sights without an Almanac
- Automatic calculation of hour angles, declination and sight reduction
- Chart plots and full results print-outs of all angles and position lines
- Stars Charts for all 59 stars giving SHA, elevation and bearing
- Star Identification from angle and bearing
- Schedule of positions of all celestial bodies
- Sun and Moon rise and set including Sun transits

This guide does not try to teach astro navigation, however it is particularly suited to students of navigation who wish to learn the methodology. You can select calculation of hour angles and declination using:

- Aries Corrections
- Polynomial Coefficients (see Compact Data in the Bibliography)
- Almanac Data - Greenwich and Sidereal Hour Angles and Declination

Knowledge of the basic theories is assumed. A bibliography is given at the end of the guide in addition to the explanations of the formulae and algorithms used by the system.

We strongly recommend that you review each of the examples in turn with this manual and make sure that you understand the results produced. Registration entitles you to support so please contact Alastair Day if you need help or more information.

Copyright © Systematic Finance 2020. All rights reserved. All intellectual contents and any derivatives or improvements on the Systematic Navigation disk are the property of Systematic Finance. The programs have been extensively tested, however, no liability whatsoever can be accepted regarding the use or accuracy of the programs and associated data. We will make every effort to correct such software errors that are found and reported to us.

| Date / Reference: | v7.0 1-Jan-2021 |
| :--- | :--- |
| Expiry Date: | 31 December 2025 |

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### 1.1 Systematic Maps - www.sysmaps.co.uk

See also Systematic Maps at www.sysmaps.co.uk for free on-line mapping provided by government and collaborative organisations. This site offers more explanation of the astro navigation program together with a number of different maps:

- UK Ordnance Survey topographical maps
- Mapbox open source world-wide maps
- French IGN topographical maps
- OpenStreetMap and German BKG topographical maps with Bing, Google, Yahoo, relief and other layers
- UK historic Ordnance Survey maps from 1888 to 1961
- Google maps with search and StreetView window
- Bing with street maps and UK 1:25000 Ordnance Survey
- Here maps with local search and routing

All the maps allow a GPS signal feed from Franson GPSGate software and are 'location aware' which positions the maps based on Wi-Fi signals. There are also other services such as search and geocoding which provide addresses and latitude/longitude positions. See the Information page at www.sysmaps.co.uk for a full specification.


Specimen maps are on the next page:

- UK Ordnance Survey
- Mapbox open source
- French IGN
- Here maps



## 2 Installation

### 2.1 Description

The system requires a computer with minimum 15.0 Mb spare hard disk capacity and sufficient RAM. The software required is Microsoft Excel 2003 (or later). Excel 2010+ is recommended.

A full pack of files for Systematic Navigation could include the following:

| Description | File Name | Approximate Size |
| :--- | :--- | ---: |
| Excel Application File | SFLNavXX.xls | $10,319,000$ |
| SysNav manual | SFLNavXX.pdf | 5,500 |
| Icon File | SFLNav.ico | 766 |
| Read Me Text File | ReadMe.txt | 6,978 |

### 2.2 Installation

Decompress the files and then set up a directory called Systematic Navigation. Copy the files to the directory and set up a link to the Excel file and manual if required.

To start Systematic Navigation, click the file icon twice quickly to load Excel and the application. A copyright box appears. Click 'OK' and the system displays a description of the information needed. See Section 3.2 for an overview map of the application and Section 4 for detailed instructions.

When you first open the application, click 'Halt' at the description dialog box and manually tab along the sheets to the end schedule, 'Version'. Enter the name and code as given to you on your invoice to register the Systematic Navigation.

## 3 Overview

### 3.1 General Principles

Out of sight of land, there are no landmarks for checking assumed or dead reckoning positions. Similarly, stand-alone GPS or GPS units in mobiles can exhibit problems or run out of battery power. Astro navigation is one method of deriving positions using observations of the Sun, Moon, Stars and Planets. The basic steps in astro navigation are:

- Taking a sight with a marine sextant from an assumed position and noting the exact time.
- Applying correction to the altitude for refraction, instrument error, height etc.
- Computing the position of the body observed (Local and Greenwich Hour Angles and Declination).
- Sight reduction - computation of the altitude and bearing at the time of sight.
- Position lines - comparing the sight reduction with the actual sight and plotting a sight line and distance from the assumed position.
- Entering further sights to derive and plot a statistical fix.

Position lines are generally assumed to be straight over distances up to a few hundred nautical miles. The observer lies along or close to each calculated position line so that the intersection of several position lines increases the accuracy of the 'fix'.

To determine the position line, the altitude of the body is observed above the horizon with a marine sextant. The observer applies corrections to the observed altitude. It can then be compared with the calculated altitude of the centre of the body as if seen from the centre of the earth with no atmosphere. Corrections include instrument or index error, height of the observer's eye above the horizon and the upper or lower limb of the body observed.


The Greenwich Hour Angle and Declination of the body need to be computed. These are equivalent to the latitude and longitude of the body in the heavens. Either tables or the Almanac can be used or this application provides an automatic method needing no input from you.

The normal method of plotting position lines is to use the intercept and azimuth. The intercept is the difference between the observed altitude and the calculated altitude represented as a distance in nautical miles. If the observed altitude is greater than the calculated altitude, the position line lies between the observer and the body. The position line is plotted at right angles to the azimuth of the body at the distance of the intercept from the estimated position - towards the body.

When the observed altitude is less than the calculated altitude, the opposite is true. The body lies away from the observer at an angle of $180^{\prime}$ plus the azimuth.

Further sights of the same body can be added to provide several position lines or alternatively different bodies along a course line. More observations increase the probability of position through the intersection of several lines. The observer can than compute a new assumed position based on the sights as a latitude/longitude position and a distance and bearing from the assumed position.

### 3.2 Systematic Navigation

The methodology described above requires the Almanac and concise mathematics plus plotting instruments to prove a position. These methods are prone to error and time-consuming.

Systematic Navigation is an Excel workbook with groups of separate 'sheets' or 'schedules'. It contains all the base data required and reduces sights and fixes positions for up to three sextant sights of the Sun, 59 navigational Stars, the Moon or the planets of Venus, Mars, Jupiter and Saturn. Data is available from 1991 and is updates in five yearly intervals as new data becomes available. It dispenses with all the manual calculation of corrected altitudes, hour angles and declination from the Almanac and the plotting of position lines on a chart.

Systematic Navigation is not intended as a complete introduction manual of astro navigation ${ }^{1}$. This manual does however contain full explanations of the methods used and lists the algorithms.


Example fix showing the dead reckoning (DR) and calculated fix positions:


[^0]
### 3.3 Overview of Systematic Navigation

This is a 'map' of the application. It identifies the main inputs, choices and flow of information to demonstrate the flexibility between automatic calculation, user choice and manual input.


For completeness this is a listing of all the schedules in Systematic Navigation. When you open the application and choose automatic entry, you enter data to dialog boxes which the system enters directly to the 'Inputs' sheet. This sheet calculates the results and retrieves data from other background schedules.

The system displays the plots on the Results, SightCharts, StarsCharts and Positions schedules.
There are two input methods: you can enter data directly to the 'Inputs' or use the dialog boxes to enter the data in stages. The dialog boxes check your inputs and should remove most input errors.

| Task | No | Option |
| :--- | :--- | :--- |
| ReadMe | 1 | On-line notes on Systematic Navigation |
| Overview | 2 | Useful map of the application (previous page) |
| Registration | 3 | 'Shareware' registration document |
| Inputs | 4 | Main input sheet and results sheet with workings |
| Results | 5 | Summary inputs and results with chart plot |
| SightCharts | 6 | Chart plot and positions plot of the Sun, Moon and Planets |
| StarsCharts | 7 | Star chart plotted in number order or by altitude, bearing or SHA |
| Positions | 8 | Calculated position of all bodies at the dead reckoning time |
| RiseSet | 9 | Sun and Moon rise and set including Sun transits. |
| Moon | 10 | Moon rise and set using Chebyshev or polynomial coefficients. |
| Altitude | 11 | Altitude by hour and day for a year for selected object. |
| Great Circle | 12 | Terrestrial navigation. |
| Aries | 13 | Background calculations. |
| Data | 14 | Derived polynomial data for the dead reckoning date |
| Version | 15 | Version data on Systematic Navigation |

$\qquad$

### 3.4 Glossary

All distances are given in (sea/nautical) miles. One nautical mile is:

| Metres | $1,852.00$ metres | $(1.85$ kilometres $)$ |
| :--- | ---: | :--- |
| Yards | $2,026.08$ yards | $(1$ metre is 1.094 yards) |
| English Miles | 1.15 miles | $(1760$ yards to the mile $)$ |

A nautical mile corresponds to one minute of latitude and is made up of ten cables; thus, sixty miles is equal to one degree of latitude. Units of longitude vary with latitude and cannot be calculated in this manner.

| Term | Explanation |
| :---: | :---: |
| GMT | Greenwich Mean Time. Synonymous in this context with Universal Time (UT). |
| Lat or B | Latitude (north = positive, south = negative). Shown as $15{ }^{\prime}$ N 12.33" or 15.2055.' |
| Long or L | Longitude (east = positive, west $=$ negative $)$. |
| GHA | Greenwich Hour Angle $=\mathrm{GHA}_{(\text {(aries })}+$ SHA measured in degrees E from $0^{\prime}$ to 360 '. |
| SHA | Sidereal Hour Angle = $360-$ Right Ascension. |
| DEC | Declination measured in degrees north (positive) and south (negative). |
| LHA | Local Hour Angle = GHA + Longitude measured in degrees E from $0^{\prime}$ to $360^{\prime}$. |
| Hs | Sextant Altitude measured by the observer's sextant. |
| I | Instrument or Index Error. |
| D | Dip of horizon (height of the observer's eye above the horizon). |
| H | Apparent Altitude = sextant altitude corrected for instrument error and dip. (Hs + I - D). |
| HP | Horizontal Parallax of Sun, Moon, Venus or Mars. |
| PA | Parallax in Altitude of Sun, Moon, Venus or Mars. (HP * COS H). |
| S | Semi-diameter of the Sun or Moon. (Add lower limb and subtract upper limb). |
| Ho | Observed Altitude $=$ apparent altitude corrected for refraction and if appropriate corrected for parallax and semi-diameter. $(\mathrm{H}-\mathrm{R}+\mathrm{PA}+\mathrm{OB} \pm \mathrm{S})$. |
| Hc | Calculated or Computed Altitude - see section 11. |
| Z | Azimuth (true), measured clockwise around the horizon from 0' to 360 '. Defined as the arc of the horizon between the meridian of a place and a vertical circle passing through a celestial body. |
| P | Intercept of a sight (Ho - Hc). Towards = positive, Away = negative. |
| R | Atmospheric Refraction. |
| T | Course or track, measured as for azimuth from $0^{\prime}$ ' to $360^{\prime}$. |
| V | Speed in knots. |

Latitude and longitude may be written in degrees with decimals or minutes. You usually enter degrees and minutes which the application converts to decimal degrees. Similarly, longitude can be converted to time since 15 ' is equivalent to one hour.

Local Mean Time is referred to as Zone Time. ZT and GMT are calculated by reference to longitude.
GMT or UT = Zone Time + west longitude or - east longitude (converted into hours i.e. $15^{\prime} \mathrm{W}=$ plus one hour).
Declination (DEC) is equivalent to the latitude of the body observed and measured in degrees north or south. For example: the Sun moves from the furthest position in the South on 21st December to the 21st June in the North.

Hour Angles are the equivalent of longitude except that longitude is measured up to 180 degrees whereas hour angles have values up to 360 degrees. Three kinds of hour angle are used to calculate positions:

- Sidereal Hour Angle (SHA) is based on a meridian line (c.f. Greenwich for longitude) and in the heavens this is the first point of Aries. The SHA is the degree's difference to Aries (the hour equivalent of the Greenwich meridian).
- Greenwich Hour Angle (GHA) is the addition of the Aries position and the Sidereal Hour Angle.
- Local Hour Angle (LHA) completes the calculation as the addition of the GHA and Longitude (West is subtracted).

Therefore $\mathrm{LHA}=\mathrm{GHA}_{(\text {Aries })}+$ SHA $+/$ - observer's longitude

## 4 Using Systematic Navigation

### 4.1 Method

Systematic Navigation incorporates two different methods of computing the Local Hour Angle and Declination of the observed body. The two methods are denoted as 'A' or 'B' throughout the model.
(A) Almanac / Calculated (A). The model will compute the position of the Sun and Moon automatically and will prompt for Almanac data on the SHA and DEC for Stars and the GHA and DEC Planets. You will find this information on the page in an Almanac containing the day of the observation.
(B) Polynomial Coefficients (B). These are assimilated from NavPac and Compact Data produced by Her Majesty's Nautical Almanac Office (HMNAO) and other sources, (referred to in this manual as Compact Data). The model calculates the GHA, declination and if applicable the horizontal parallax and semi diameter of the body observed. The model computes the DEC and GHA and adds the longitude to convert to LHA (Local Hour Angle).

The most convenient method for calculating GHA and Declination for each body is shown below. The model will prompt you for the method to be used on all sights. Similar to Methods 'A' and 'B', the celestial bodies are referred to throughout the model by their numbers below:
(1) Sun: Under 'A' GHA and DEC are calculated for 1989-2025, and under Method 'B' the coefficients for 1991-2025 are contained in the model. If you enter an observation for another year, Method 'B' will prompt you to input the coefficients applicable to the month and year.
(2) Stars: The model requires the SHA and DEC under Method 'A' however the data under Method 'B' for the years 1991-2025 are contained in the model. The apparent position of the Stars does not vary month to month and therefore the coefficients are contained on a series of five-year tables.
(3) Moon: Method 'A' and 'B' are calculated for 1989-2025. Method 'B' uses monthly Chebyshev or polynomial coefficients contained in the model.
(4) Planets: These are denoted as $4=$ Venus, $5=$ Mars, $6=$ Jupiter, $7=$ Saturn. Under Method 'A' the Greenwich Hour Angle and the Declination together with hourly corrections must be input. The polynomial coefficients for 1991-2025 are in the model for Method 'B'.

The above provides some flexibility in the model to test the different methods and the results will be very similar. To reduce the complexity of the above, you can decide to compute the GHA and DEC automatically and in this case the routine will choose either ' A ' - Calculated / Almanac or 'B' - Compact Data as follows:
(1) Sun: Method 'B' for 1991-2025 otherwise Method 'A'. The model derives the coefficients for 1991-2025 and will also calculate the semi-diameter accurately as opposed to using the single figure of 16 " used in Method 'A'. This will account for any resulting small differences between the two methods.
(2) Stars: Method 'B' (polynomial coefficients provided for the years 1991-2025).
(3) Moon: Method 'A' and ' $B$ ' with no inputs needed. Method ' $B$ ' for the years 1991-2025 is more accurate using the Chebyshev coefficients.
(4) Planets: Method 'B' (polynomial coefficients provided for the years 1991-2025).

### 4.2 Procedure

(1) Double click Systematic Navigation in the program group or load SFLNavXX.xIs and the application displays a copyright box and requests confirmation of the working directory and language for the reports.

If the system displays the 'circular errors' box, press 'OK' and continue. This is merely informing you that the workbook may contain circular arguments and needs the Excel calculation option set to iteration. If you start the application from an icon, the system should suppress this message. The system sets up the calculation method as it opens so you need take no further action.

```
Systematic Navigation: Copyright ? }
'Registered' version of Systematic Navigation: 31-Dec-2025.
All rights reserved. All intellectual contents and any derivatives or improvements
are the property of Systematic Finance Limited. The application has been
extensively tested, however no liability can be accepted regarding the accuracy
of the application and its associated data.
(c) Crown Copyright and/or database rights.
Reproduced by permission of the Controller of Her Majesty's Stationery Office
and the UK Hydrographic Office (www.ukho.gov.uk).
Select language for reports and charts: Language
                                    (O) English
Deutsch
C:\Users\Alastair Day\Desktop\Documents
(c) Systematic Navigation
Orchard House, Green Lane
Press 'OK' to continue
```



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Version 7.0 1-Jan-2021
```

(2) Press 'OK' and the system displays the Main Menu showing the data contained in the model. Use the control to select Inputs directly or press 'Automated Data Entry' to enter data via dialogue boxes.

The options are:

| ReadMe | Background notes on installation and operation of the Application |
| :--- | :--- |
| Overview | Graphical overview of the Application |
| Registration | Registration document together with details on how to register the <br>  <br> Application |
| Inputs | Enter details of up to three sights |
| Results | View summary results and chart plot |
| Sight Charts | View large scale chart plot |
| Stars Charts | View star charts in SHA, altitude or bearing order |
| Positions | View hour angles and declination for position, date and time in Inputs |
| RiseSet | View sun and moon rise and set for position, date and time in Inputs |
| Aries | Background calculations |
| Data | Data for the date and time in Inputs |
| Version | Version information and entries for registration codes |

Systematic Navigation

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(3) Press 'Automated Data Entry' and the system displays the Main Menu showing the data contained in the model. Use 'Halt' to stop here and enter all data manually to the Input sheet. If you halt at this point, the system does not recalculate and you should use the button or F9 to update the model.

Automated Data Entry will start a macro described in the following pages with input boxes for the DR position and each of the sights. Any data in the model will be entered in the boxes as they open. If you do not press this button use the combo box to jump to individual sheets or tab along the bottom in Excel. You enter all data on the Inputs sheet and the calculations are used on all the other sheets and charts. The following pages show the automatic sequence.

Reset to top of page resets all sheets to the top ready for saving.
In Excel 2003 you can use Custom Toolbars and Excel Toolbars to toggle between the application and Excel toolbars.

```
Systematic Navigation: Information
    Astro Navigation fixes positions with up to three sextant sights by two distinct methods using
    (1) Sun
    (2) Stars: 59 Navigational Stars
    (3) Moon
    (4) Planets:Venus, Mars, Jupiter and Saturn
    Input:
    (1) DR Latitude / Longitude, Date, Time, Course and Speed
    (2) Body Observed, Time, Observed Altitude, U / Lower Limb and Height
    (3) Declination / Greenwich Hour Angle (GHA)
    A : Calc. : Sun and Moon : Almanac needed for Stars - SHA and Declination
    : Planets' GHA and Declination plus Hourly variation
    B : Polynomial Coefficients from 'Compact Data for Navigation and Astronomy for 1991-2005'
    : No inputs for the Sun, Stars, Planets
    : Coefficients needed for the Moon from 'Compact Data'
    No inputs for the Sun / Moon on Method "A" and the Sun / Stars / Planets on Method "B"
    Azimuth / Intercept displayed : Fix given for two sights or more
    Press HALT or OK to continue (c) Systematic Navigation Version 7.0 1-Jan-2021
    \square \text { HALT}
```

    \(? \quad \times\)
    4) Press 'OK' and the system requests you to select general options for the sights. These are set to true and they must be clicked to de-select them. The options are:
(a) Keep DR (Dead Reckoning) position and time
(b) Calculate GHA and DEC automatically ${ }^{2}$
(c) Keep existing sight results.

Clicking (a) or (c) will cancel the sights held in the system. If the selection is left untouched, the system will load the currently saved entries into the dialog boxes for cancellation, editing and amendment. Sight Data can be changed and this option does not prevent future editing.

Clicking (b) allows you to choose the method of computing the GHA and DEC.
Select 'OK' to continue or 'Re-Do' to return to the previous screen.

[^1](5) A box requesting the DR position and zone time together with any course and speed between the DR position and the sights (if applicable). You should also enter the number of sights (maximum three). However, if one or two are entered and you chose the retention of current data, any sight numbers above the number of sights chosen will be erased when calculating fixes. Press 'OK' to continue or 'Re-Do' to return to the Main Menu.

Note: the zone time is calculated with reference to longitude and no account is taken of any local time differences e.g. winter and Summer time.

For stars, there is a subroutine for identifying stars or using their number to check the attitude and bearing. See the 'Stars' section 7 below for a full explanation of the three options.

(6) The model prompts you for the body observed and the zone time or local mean time. GMT is calculated by reference to longitude e.g. $100^{\prime} \mathrm{W}=100^{\prime} \mathrm{W} /\left(360^{\prime}\right.$ per day $/ 24$ hours $)=6.67$ hours rounded to 7.0 hours. If the calculation of GHA and DEC is set to automatic, as below, the explanation is dimmed and the relevant method is shown. 'A' for Calculated/Almanac and 'B' for Compact Data. Press 'OK' to continue or 'Re-Do' to return to the Main Menu.

(7) Input the Observed Angle. Input the angle in degrees and minutes together with the height of the user's eye i.e. the height above sea level. There are also prompts for the index or instrument error and whether the upper or lower limb was observed. Any items not required for the body observed will be dimmed. Press 'OK' to continue of 'Halt' to stop for manual input. If you select the latter, the system will enter all data so far entered and recalculate the model.


(8) The system now calculates GHA and DEC or prompts you for Almanac data for the day of the sight. If you opted to control the calculation of the GHA and DEC, a box reminds you how the ephemeris is being calculated or alternatively the system asks you for data such as the SHA and DEC.
(9) The information to calculate a position line is now complete and system prompts for:
(a) View result for this sight before continuing with other sights
(b) Increase the number of sights to a maximum of three
(c) Enter no more sights and view final results (and fix if two or more sights entered)
(d) Continue with more sights

The default setting continues with more sights if the sight number is less than the total entered on commencement. If (a) is selected then the system calculates, and the object bearing and azimuth are displayed together with the computed latitude and longitude position of the intercept. The model allows you to re-enter the sight details or press 'OK' to accept this result and continue with the next sight. When all sights have been entered, the options are greyed and the model defaults to calculating a fix.

| Systematic Navigation : Options |  | $?$ | $\times$ |
| :--- | :--- | :--- | :--- |
| Information now entered for sight number | 1 |  |  |
| Select option |  |  |  |
| View result for this sight |  |  |  |
| Increase Number of sights |  |  |  |
| Enter no more sights and view results and fix |  |  |  |
| Continue with more sights |  |  |  |
| OK |  |  |  |

(10) The system enters all the data on the 'Inputs' sheet as shown on the next page. It is divided into:

- DR Position
- Bodies observed, time and method of ephemeris calculation
- Altitude correction
- GHA, LHA and DEC
- Azimuth and Intercept
- Calculated position and confidence ellipse

Further pages detail the calculations for GHA and LHA, DEC, Observed Altitude (Ho), Computed Altitude (Hc) and the derivation of the statistical fix and error probability.

| DR Position: | , |  |  | Calculated Position: |  |  |  | English | English |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DR Latitude |  | $50^{\prime} \mathrm{N}$ | 35.14 " |  | $50^{\prime} \mathrm{N}$ | 31.71 " |  | Confidence | 95.00\% |
| DR Longitude |  | $4^{\prime} \mathrm{W}$ | -55.09 " |  | $4^{\prime} \mathrm{W}$ | 58.57 " |  | Ellipse |  |
| DR Zone Date |  | 31-Mar-23 | Friday |  | Distance | 4.083 mls |  | Latitude | 3.22 mls |
| Zone/GMT |  | 9:00:00 | 09:00:00 GMT |  | Bearing | 213.83 T |  | Longitude Bearing | $\begin{aligned} & 8.16 \mathrm{mms} \\ & 40.38 \mathrm{~T} \end{aligned}$ |
| Course / Speed |  | 0.00 T | 0.00 kn |  |  |  |  |  |  |
|  | Sight \# 1 |  |  | Sight \# 2 |  |  | Sight \# 3 |  |  |
| Which Sight |  | 3 | Moon |  | 2 | Star |  | , | Sun |
| Method : 'A' or 'B' |  | A | Calculated |  | B | Polynomial |  | B | Polynomial |
| Actual Sight Time |  | 3:00:00 | 03:00:00 GMT |  | 4:28:32 | 04:28:32 GMT |  | 8:55:00 | 08:55:00 GMT |
| Time Diff. / Miles |  | 6:00 hrs | 0.00 mls |  | 4:31 hrs | 0.00 mls |  | 0:05 hrs | 0.00 mls |
| Revised DR Position |  | $50^{\prime} 35.1^{\prime \prime} \mathrm{N}$ | $4^{\prime} 55.1^{\prime \prime} \mathrm{W}$ |  | $50^{\prime} 35.1{ }^{\prime \prime} \mathrm{N}$ | $4^{\prime} 55.1^{\prime \prime} \mathrm{W}$ |  | $50^{\prime} 35.1^{\prime \prime} \mathrm{N}$ | $4^{\prime} 55.1{ }^{\text {" }} \mathrm{W}$ |
| DR Star Altitude ' |  | $0.00{ }^{\prime}$ | 0 |  | 0.00' | 0 |  | 0.00' | 0 |
| DR Star Bearing ' |  | 0.00 E | 0 |  | 0.00 E | 0 |  | 0.00 E | 0 |
| Star Number |  | 0 | 0 | Input Star No | 40 | Kochab |  | 0 | 0 |
| DR Alt. / Bearing |  | $11^{\prime} 26.4{ }^{\prime \prime}$ | $295{ }^{\prime \prime} 14.78^{\prime \prime}$ |  | $63^{\prime} 46.75^{\prime \prime}$ | 343' $7.84{ }^{\prime \prime}$ |  | $26^{\prime} 18.62$ | $118^{\prime} 24.18^{\prime \prime}$ |
| Observed Angle | $\begin{gathered} 10^{\prime} \\ 0.00^{\prime \prime} \end{gathered}$ |  | 30.00 " | $\begin{gathered} 63^{\prime} \\ 0.00^{\prime \prime} \end{gathered}$ |  | 49.00 " | $\begin{gathered} 26^{\prime} \\ 0.00^{\prime \prime} \end{gathered}$ |  | 10.00 " |
| Index Error: Minutes |  |  |  |  |  |  |  |  |  |  |  |
| On/Off the Arc: $\mathrm{N} / \mathrm{F}$ |  | F |  | Off Arc | Calc. HP/SD | F | Off Arc | $\begin{gathered} F \\ 6.00 \mathrm{mtr} \end{gathered}$ |  | Off Arc |
| Height of User's Eye |  | 6.00 mtr | 6.00 mtr |  |  |  |  |  |  |  |  |
| Upper / Lower Limb |  | L | Lower$54.1{ }^{\prime \prime} / 14.7^{\prime \prime}$ | L |  | Lower$0^{\prime \prime}$ | Calc. HP/SD | L | Lower $16^{\prime \prime}$ |  |
| Moon HP/SD |  | 0.00 " |  | 0.00 " |  |  |  | 0.00 " |  |  |
| Corrected Altitude | , | $11^{\prime} 28.38^{\prime \prime}$ |  | $63^{\prime \prime} 44.21^{\prime \prime}$ |  |  | $26^{\prime} 19.85^{\prime \prime}$ |  |  |  |  |
| Calc Moon DEC |  | $0^{\prime} \mathrm{N}$ | 0.00 " | Calc. DEC |  | $0^{\prime} \mathrm{N}$ | 0.00 " | Calc. DEC | $0^{\prime} \mathrm{N}$ | 0.00 " |
|  |  | $0{ }^{\prime}$ | 0.00 " |  | $0^{\prime}$ | 0.00 " | 0 ' |  | 0.00 " |  |
|  |  | 0 ' | 0.00 " |  | 0 ' | 0.00 " |  | 0 ' | 0.00 " |  |
| Moon Declination | , | $24^{\prime} 44.98^{\prime \prime}$ | North | Star DEC | 74'3.4" | North | Sun DEC | $4^{\prime} 6.71{ }^{\prime \prime}$ | North |  |
| Calc Moon GHA |  | $0^{\prime} \mathrm{E}$ | 0.00 " | Calc. GHA | 0 'E | 0.00 " | Calc. GHA | 0 'E | 0.00 " |  |
|  |  | $0{ }^{\prime}$ | 0.00 " |  | $0{ }^{\prime}$ | 0.00 " |  | $0^{\prime}$ | 0.00 " |  |
|  |  | 0 ' | 0.00 " |  | 0 ' | 0.00 " |  | 0 ' | 0.00 " |  |
| Moon GHA / LHA |  | 107 $26.94{ }^{\prime \prime}$ | $102^{\prime} 31.85{ }^{\prime \prime}$ | Star LHA | $32^{\prime \prime} 44.58^{\prime \prime}$ | $27^{\prime \prime} 49.49^{\prime \prime}$ | Sun LHA | $312^{\prime \prime} 40.96^{\prime \prime}$ | $307{ }^{\prime \prime} 45.87{ }^{\prime \prime}$ |  |
| Azimuth / Bearing |  | 295' 14.78" | 295' 14.78' |  | 343' $7.84{ }^{\prime \prime}$ | 163' $7.84^{\prime \prime}$ |  | 118' $24.18^{\prime \prime}$ | 118' $24.18^{\prime \prime}$ |  |
| Intercept: Miles |  | 1.99 mls | Towards |  | 2.53 mls | Away |  | 1.23 mls | Towards |  |
| Calc. Position |  | $50^{\prime} 36^{\prime \prime} \mathrm{N}$ | 4' $57.8^{\prime \prime} \mathrm{W}$ |  | $50^{\prime} 32.8{ }^{\prime \prime} \mathrm{N}$ | 4' $54{ }^{\prime \prime} \mathrm{W}$ |  | $50^{\prime} 34.6$ "N | 4' 53.5 "W |  |

(11) The screen shows a 'best-fit' calculated position with the latitude and longitude and the distance and true bearing from the DR position. The model uses the least squares method from Compact Data et al. to produce a most probable position within a confidence ellipse of $95 \%$. To produce an accurate fix, three sights are normally required with some angle between them to provide a 'good cut'. A summary of the position lines for other sights is included.

If any sights are inaccurate such that the intercept is greater than 500 miles, the system will not compute a fix and will display an error message. Similarly, the system will not compute a fix with only one sight although it will derive the latitude longitude position of the observation from a single azimuth and intercept.

Press 'OK' to continue to print, view and 'Re-Do' options. The following show the background calculations on the two other pages on the Inputs schedule.

This is the first page of workings showing the Greenwich Hour Angle, Declination, Polynomial Coefficients (if used) and the corrected altitude. The methodology follows The Nautical Almanac. These figures are summarised on the first page and on the Results schedule.

You can improve the position fix by selecting iteration on the Inputs sheet. This will attempt to converge and improve the solution.

(A) GHA and DEC Workings

| Sun DEC \& GHA | Sight (1) | 6.00 hrs | Sight (2) | $\mathbf{1 8 . 0 0} \mathbf{~ h r s ~}$ | Sight (3) |
| :--- | ---: | ---: | ---: | ---: | :---: |
| Sun DEC | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ | $1.000^{\prime}$ |
| Convert to Radians | 0.000 | 0.000 | 0.000 | 0.000 | 0.017 |
| V | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| DEC : E | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Declination in Degrees | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ |
| X | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Add to 180' | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ |
| Calculated Sun GHA | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ | $0.000^{\prime}$ |
| LHA Time | $0: 00: 00$ |  | $0: 00: 00$ |  | $0: 00: 00$ |

Star DEC and GHA

| Star | Sight (1) | Sight (2) | Sight (3) |
| :--- | :---: | :---: | :---: |
| DEC Degrees | $0^{\prime}$ | $0{ }^{\prime}$ | 0 |
| Minutes | $0.00^{\prime \prime}$ | 0.00 | 0.00 |
| Decimal DEC | 0.0000 N | 0.0000 N | 0.0000 N |
| SHA | 0 E | 0 E | 0 E |
| Minutes | $0.00^{\prime \prime}$ | 0.000 | 0.000 |
| Decimal SHA | 0.0000 E | 0.0000 E | 0.0000 E |
| SHA + Calc GHA Aries | 0 | 0 | 0 |
| Calc Star GHA | 0.0000 E | 0.0000 E | 0.0000 E |

Polynomial Coefficients

| Sun and Planets | Sight (1) |  | Sight (2) |  |  | Sight (3) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | GHA DEC |  | GHA | DEC |  | GHA | DEC |
| Coefficient 0 | 0.00000000 .0000000 |  | 237.2095000 | 74.0706000 |  | 11.7895100 | -8.1488000 |
| Coefficient 1 | 0.000000000 .0000000 |  | 1.0000017 | -0.0000131 |  | 0.0956700 | 12.0737000 |
| Coefficient 2 | 0.000000000 .0000000 |  | -0.0162000 | -0.0033000 |  | 0.0811200 | 0.9736000 |
| Coefficient 3 | 0.000000000 .0000000 |  | 0.0117000 | -0.0046000 |  | -0.0388300 | -0.5207000 |
| Coefficient 4 | 0.000000000 .0000000 |  | 0.0000000 | 0.0000000 |  | 0.0045100 | -0.0228000 |
| Check Sum | 0.00000000 .0000000 |  | 238.2050017 | 74.0626869 |  | 11.9319800 | 4.3550000 |
| Days: X | $0.0000 \quad 0.0000$ |  | 0.9746 | 808.4147 |  | 0.9804 | 808.5971 |
| Calculated | 0.0000' $0.0000^{\prime}$ |  | 1045.6097' | $74.0566^{\prime}$ |  | 11.9288' | $4.1118^{\prime}$ |
| GHA and DEC | $0.0000^{\prime} \quad 0.0000^{\prime}$ |  | 1112.7430' | $74.0566^{\prime}$ |  | $312.6827^{\prime}$ | 4.1118' |
| Coefficient A0 | 0.00000 Polar Stars on | 0.0000 | 0.00000 | Polar Stars ont | $0.000{ }^{\prime}$ | 0.26910 | Polar Stars only |
| Coefficient A1 | 0.00000 C. Alt. | 0.0000 | 0.00000 | C. Alt. | $0.000{ }^{\prime}$ | -0.00230 | 0.0000' |
| Check Sum | 0.00000 | 0.0000 | 0.00000 |  | $0.000{ }^{\prime}$ | 0.26680 | $0.0000^{\prime}$ |
| SemiDiameter | 0.0000' | 0.0000 | 0.0000' |  | $0.000{ }^{\prime}$ | 0.2668' | $0.0000^{\prime}$ |
| S-D Minutes | 0.00" Azimuth | 0.0000 | 0.00" | Azimuth | $0.000{ }^{\prime}$ | 16.01 " | $0.0000^{\prime}$ |

(B) Calculated GHA and DEC

| GHA | Sight (1) | Sight (2) | Sight (3) |
| :--- | :---: | :---: | :---: |
| Moon GHA | 0.000 E | 0.000 E | 0.000 E |
| Mean Variation | $0.0000^{\prime}$ | $0.00000^{\prime}$ | $0.0000^{\prime}$ |
| Correction | $0.0000^{\prime}$ | $0.0000^{\prime}$ | $0.0000^{\prime}$ |
| Moon GHA | $107.4609^{\prime}$ | $32.7430^{\prime}$ | $312.6827^{\prime}$ |
| GHA+Long. | $102.5428^{\prime}$ | $27.8249^{\prime}$ | $307.7646^{\prime}$ |
| Final LHA | $102.5428^{\prime}$ | $27.8249^{\prime}$ | $307.7646^{\prime}$ |
| Declination |  |  |  |
| Moon DEC | 0.000 N | 0.000 N | 0.000 N |
| Mean Variation | $0.0000^{\prime}$ | $0.0000^{\prime}$ | $0.0000^{\prime}$ |
| Variation | $0.0000^{\prime}$ | $0.0000^{\prime}$ | $0.0000^{\prime}$ |
| Moon Declination | $24.7514^{\prime}$ | $74.0566^{\prime}$ | $4.1118^{\prime}$ |

(C) Corrected Altitude (Decimals)

| Altitude | Sight (1) |  | Sight (2) |  | Sight (3) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Observed (Hs) |  | $10.5000^{\prime \prime}$ |  | $63.8167^{\prime}$ |  | $26.1667^{\prime}$ |
| Index Error (I) | 0.0000' |  | 0.0000' |  | 0.0000' |  |
| DIP - Height ( $\mathrm{D}=0.0293 *$ SqrtH) | -0.0718" |  | -0.0718' |  | -0.0718" |  |
| Apparent Altitude ( $\mathrm{H}=\mathrm{Hs}+1-\mathrm{D}$ ) |  | 10.4282 |  | 63.7449' |  | 26.0949' |
| Ro $=0.0167 / \tan (\mathrm{H}+7.32)(\mathrm{h}+4.32)$ ) | $0.0865^{\prime}$ | 0.0880' | 0.0082 | 0.0080' | 0.0337 | $0.0331{ }^{\prime}$ |
| $\mathrm{f}=0.28{ }^{\text {Pressure }}$ (Temp +273 ) | 0.9993' |  | 0.9993' |  | 0.9993' |  |
| Refraction ( $\mathrm{R}=\mathrm{Ro}^{*} \mathrm{f}$ ) |  | 0.0865 ${ }^{\prime}$ |  | 0.0080' |  | $0.0331{ }^{\prime}$ |
| Oblateness of Earth (OB) |  | -0.0017' |  | 0.0000' |  | $0.0000^{\prime}$ |
| Parallax (HP) | $0.9027^{\prime}$ |  | 0.0000' |  | 0.0024' |  |
| Parallax Altitude ( $\mathrm{PA}=\mathrm{HP}^{*} \cosh$ ) |  | 0.8878' |  | 0.0000' |  | 0.0022 |
| Semi Diameter (S) |  | 0.2459' |  | 0.0000' |  | $0.2668^{\prime}$ |
| Corr. Altitude ( $\mathrm{Ho}=\mathrm{H}-\mathrm{R}+\mathrm{PA}+\mathrm{S}$ ) |  | 11.4737 |  | $63.7369^{\prime}$ |  | $26.3308^{\prime}$ |

The third page of workings derive the intercept and azimuth from the computed angle and the fix position using the method of 'least squares'. It also calculates the standard deviation and the estimated position error.
(D) Sight Reduction

| Altitude | Sight (1) | Sight (2) | Sight (3) |
| :---: | :---: | :---: | :---: |
| Computed Altitude ( Hc ) | $0.1996^{\prime}$ | 1.1132 | 0.4592' |
| Angle in Degrees | 11.4342' | $63.7790^{\prime}$ | $26.3105^{\prime}$ |
| Azimuth Angle | $1.1300{ }^{\prime}$ | 0.2944' | $2.0665^{\prime}$ |
| Angle in Degrees | $64^{\prime} 44.63$ " | $16^{\prime} 52.16^{\prime \prime}$ | $118{ }^{\prime} 24.18^{\prime \prime}$ |
| Corrected Azimuth (Z) | $295.2561{ }^{\prime}$ | $343.1306{ }^{\prime}$ | 118.4031' |
| Angle in Degrees | $295{ }^{\prime} 15.37^{\prime \prime}$ | 343' $7.84{ }^{\prime \prime}$ | $118^{\prime} 24.18^{\prime \prime}$ |
| Latitude Difference (P) | $0.0395^{\prime}$ | $0.0421^{\prime}$ | 0.0204 |
| Latitude as Miles | 2.37 mls | 2.53 mls | 1.22 mls |
| Towards/Away | Towards | Away | Towards |


| Position | Sight (1) |  |  | Sight (2) |  | Sight (3) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Azimuth 1 | $295.256^{\prime}$ | 1 | $295.256^{\prime}$ |  |  |  |  |
| Course | 0.00 T |  |  |  |  |  |  |
| Distance2 | $0.0000^{\prime}$ |  |  |  |  |  |  |
| U=90+G | $385.256^{\prime}$ |  |  |  |  |  |  |
| Take out Excess 360 | 565.256' | 205.256' |  |  |  |  |  |
| U | 0.000 | 0.000' |  |  |  |  |  |
| W+U | 0.040' | 0.040' |  |  |  |  |  |
| Take out Excess 360 | 475.256 | 115.256' |  |  |  |  |  |
| Latitude | 50.586 N | 50 N | 35.14 " |  |  |  |  |
| Longitude | 4.918 W | 4 W | -55.09 " |  |  |  |  |
| True Azimuth Bearing (Z) | 295.256 T | 2.37 mls |  | 163.131 T | 2.53 mls | 118.403 T | 1.22 mls |
| Plot Position / Direction | 025.26 T | NW |  | 073.13 T | SE | 028.40 T | SE |
| Distance | -2.14 mls | 1.01 mls |  | 0.73 mls | -2.42 mls | 1.07 mls | -0.58 mls |
| Bearing Miles | 2.144 W | 1.011 N |  | 0.733 E | 2.419 S | 1.075 E | 0.581 S |
| Latitude/Longitude | 0.054 W | 0.016 E |  | 0.018 E | 0.039 S | 0.027 E | 0.009 S |
| Revised Fix Position | 4.972 W | 50.602 N |  | 4.900 W | 50.547 N | 4.891 W | 50.576 N |
| Minutes | 58.3277 | 36.1068 |  | 53.9770 | 32.8140 | 53.4613 | 34.5782 |

(F) Fix : Method of Least Squares

|  |  |  |  | (G) Estimated Position Error |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A | 1.32410 | A + C $=$ Sights | 3.000 | Standard Devilation | 2.3784 mls |
| B | -1.08200 | No of Sights | 3 | Deviation Longitude | 2.6730 mls |
| C | 1.67590 |  |  | Deviation Latitude | 3.0072 mls |
| D | -0.03314 |  |  | $2 \times$ Tan | $6.151{ }^{\prime}$ |
| E | -0.00559 |  |  | Atan /2 = Ellipse Azimuth | 40.383' |
| F | 0.00375 |  |  | Probability P=0.95 Scale Fact | 2.4477 |
| $\mathrm{G}=\mathrm{AC}-\mathrm{B}^{\wedge} 2$ | 1.04834 |  |  | A : X | 9.1617 mls |
|  |  |  |  | B: Y | 3.6132 mls |


(12) The system displays an options box repeating the Calculated Position and requesting the next action:

1. View input sheet and halt for manual input.
2. View results and chart plot.
3. View chart plot and sights charts.
4. Update and sort stars charts by SHA, altitude or bearing.
5. View stars charts.
6. View Sun, Moon, Planets and Stars positions.
7. View Sun and Moon rise and set and Sun transits.
8. View background data and Aries corrections.
9. View polynomial coefficients for the date of the sights.
10. Re-Run some or all of the sights.
11. Halt for manual input.
12. Quit Astro Navigation and return to Windows with an option to save files.

If you press 'Halt', then the system displays the Welcome sheet. Use the tabs at the bottom to activate any of the other sheets. You can review all data on the Inputs sheet.

| Systematic Navigation : Options |
| :--- | :--- | :--- |
| Position calculated as Fix : 50 ' $31.71^{\prime \prime} \mathrm{N} 4^{\prime} 58.57^{\prime \prime} \mathrm{W}$ |
| Distance from DR Position $\quad 4.08 \mathrm{Mls}: 213.83 \mathrm{~T}$ |
| Option |
| View Inputs and Halt for manual input |
| View Results and Chart Plot |
| View Chart Plot and Sight Charts |
| Update Star Charts by Atitude or Bearing |
| View Star Charts |
| View Sun, Stars, Moon and Planet Positions |
| View Sun and Moon Rise and Set |
| View Background Data and Aries Corrections |
| View Polynomial Coefficients |
| Re-run Some or All Sights |
| Halt |
| Exit Systematic Navigation with save options |
| Select an Option and Press 'OK' |

(13) Systematic Navigation will halt for you on the chosen schedule for you to review the results. If you want to reenter the sights, you can press the 'Main Menu' buttons on the schedule or select 'Main Menu' from the pulldown menus.

Press the button to save the results sheet with its chart plot to a new file. The system will prompt you for a name, but the default is Year-Month-Day.xls i.e. '23Mar31.xls'. This way you can keep a full record of the inputs, intermediate calculations and results.
(14) You have the choice of chart plots or a combined results and chart plot. Examples of the Results sheet are in the worked examples. These are example chart plots from the SightCharts schedule for 31 March 2023 at GMT 9:0:0 from an assumed position of 50 'N 35 " 4 'W 55.09":


There is also a plot of the Sun, Moon and Planets on the SightCharts schedule:



A further sheet provides a plot of the relative bearing of the fix from the DR position.


The following sections provide an explanation of each body by method with the inputs required and the options available at each stage. If 'Automatic Calculation' is left selected (see Section 4.2) Systematic Navigation will compute ephemeris without recourse to you for any data inputs. The following sections assume that you have chosen to select the manual method of derivation of GHA and DEC.

## 5 Sun

### 5.1 Method A - Aries

Select 'A' and the routine will move to the Observed Angle and thereafter the system displays a box informing you that the GHA and Declination are automatically calculated. Press 'OK' to continue and the system displays the option box to denote the end of the required inputs for the sight.

Example: The GHA and DEC of the Sun on October 22, 1996 at GMT 21:43:25³

| Sun GHA and DEC | Calculations |
| :--- | :--- |
| Sun DEC U | $288.723^{\prime}$ |
| V | 209.770 |
| DEC : E | -0.199 |
| Declination in Degrees | $\mathbf{- 1 1 . 3 9 2 0 ^ { \prime }}$ |
| X | 0.483 |
| Add to $180^{\prime}$ | $468.723^{\prime}$ |
| Calculated Sun GHA | $509.760^{\prime}$ |
| Sun GHA | $\mathbf{1 4 9 . 7 6 0 0}{ }^{\prime}$ (removing multiples of $\mathbf{3 6 0} \mathbf{}^{\prime}$ ) |

The above uses two annual update quantities P and Q which are located on a look-up table on the Aries schedule. These are the mean anomaly on day 0 of the year and the earth's longitude at perihelion. The values for 1996 are -3.9212 and 77.1260 respectively.

A further variable $B$ is the decimal time from day 0 of the year to the GMT sight time where hours of the day are also expressed as decimals.

Example: 22 October 1996 at GMT 21:43:25

$$
22 \text { October 1996-0 January } 1996=296 \text { days }
$$

GMT 21:43:25 $=(21.723611 / 24)=0.905150$

$$
\mathrm{B}=296 \text { days }+0.905150 \text { hours }=296.905150
$$

The algorithms used by the model are:
(1) DEC

$$
\begin{aligned}
& \mathrm{U}=(0.9856 * \mathrm{~B})+\mathrm{P} \\
& \mathrm{~V}=\mathrm{U}+(1.916 * \sin \mathrm{U})+(0.02 * \sin (2 * \mathrm{U}))-\mathrm{Q} \\
& \mathrm{DEC}=\operatorname{Asn}(0.3978+\sin \mathrm{V})
\end{aligned}
$$

(2) GHA

$$
\begin{aligned}
& \mathrm{X}=\operatorname{Atn}(0.9175 * \tan \mathrm{~V}) \\
& \text { If sign }(\sin \mathrm{X})<>\operatorname{sign}(\sin \mathrm{V}) \text { then } \mathrm{U}=\mathrm{U}+180 \\
& \mathrm{GHA}=360 *(\mathrm{~B}-\text { Integer }(\mathrm{B}))+\mathrm{U}-\mathrm{X}-180-\mathrm{Q}
\end{aligned}
$$

If necessary, remove multiples of $360^{\prime}$ to place the result in the range 0 to $360^{\prime}$.
(3) Semi-diameter

The model uses a standard semi-diameter for the Sun of $16^{\prime \prime}\left(0.266667^{\prime}\right)$

[^2]
### 5.2 Method B - Polynomial Coefficients

The procedure is automatic as 'A' above. Note that the information box on the calculation is not displayed if the user has selected the calculation to automatic ('B'). For years other than 1991-2025, the model will request the polynomial coefficients from for the relevant month from Compact Data.

This is the same example as above and the answers are very similar. The coefficients are selected from the tables for the month and year. The semi-diameter is also calculated at 16.11 ".

| Sun GHA and DEC | GHA | DEC |
| :---: | :---: | :---: |
| a 0 | 12.1661800 | -2.8211000 |
| a 1 | 0.1757000 | -12.4213000 |
| $\mathrm{a}_{2}$ | -0.0443100 | 0.2145000 |
| a3 | -0.0241800 | 0.5750000 |
| a 4 | 0.0000700 | 0.0070000 |
| Check Sum | 12.2734600 | -14.4459000 |
| Days: X | 0.7158 |  |
| Calculated | 12.2604' | -11.3895' |
| GHA and DEC | $509.7600{ }^{\prime}$ | -11.3895' |
| GHA (Removing multiples of $360^{\prime}$ ) | $149.7600^{\prime}$ |  |
| $\mathrm{a}_{0}$ | 0.26670 |  |
| $\mathrm{a}_{1}$ | 0.00240 |  |
| Sum | 0.26910 |  |
| Semi-diameter in degrees | $0.2684{ }^{\prime}$ |  |
| Semi-diameter in Minutes | 16.11" |  |

The calculations in the model using the coefficients are:

$$
\text { Time variable x = (d + GMT / } 24 \text { ) / } 32 \text {. }
$$

d is the day in the month and GMT the universal time in hours.
Using the example in the previous section: $[22+(21.7236 / 24)] / 32=0.715786$
Using x, (GHA - GMT) in hours and DEC in degrees are derived from this expression:

$$
\mathrm{a}_{0}+\left(\mathrm{a}_{1} * \mathrm{x}\right)+\left(\mathrm{a}_{2} * \mathrm{x}^{2}\right)+\left(\mathrm{a}_{3} * \mathrm{x}^{3}\right)+\left(\mathrm{a}_{4} * \mathrm{x}^{4}\right)
$$

This can be rewritten for use with pocket calculators:

$$
\left(\left(\left(a_{4} * x+a_{3}\right) * x+a_{2}\right) * x+a_{1}\right) * x+a_{0}
$$

You can convert the GHA in hours to degrees by adding GMT and multiplying the result by 15 to convert from hours to degrees.

The semi-diameter is calculated using the expression $\mathrm{S}=\mathrm{a}_{0}+\left(\mathrm{a}_{1} * \mathrm{x}\right)$

## 6 Stars

### 6.1 Method A - Almanac

The system displays a box requesting the Sidereal Hour Angle and Declination for the day of the sight. Daily/hourly corrections are dimmed since these are only needed for the Planets. The user therefore need only input two numbers for this method. It can be used to check any sight using the Compact Data where the result appears to be inaccurate.

Example: The GHA and DEC of Aldebaran (10) on 3 February 1996 at GMT 17:23:17 ${ }^{4}$.
To derive the star's GHA, the system calculates the GHA of Aries as:

$$
\mathrm{GHA}_{(\text {Aries })}=\mathrm{R}+(360.985647 * \mathrm{~B})
$$

B is the number of decimal days from day 0 of the year to the time of sight. R is the Aries coefficient constant for the year and gained from a look-up table on the Aries schedule. In this example Aries is 33.9998.

GHA (Aries) is added to the SHA, 291.0733', to produce the GHA for the star as $325.0732^{\prime}$.
The model uses the Declination you input since this variable changes very slowly. The almanacs contain a list of the 57 navigational stars plus the polar stars Polaris (58) and Octantis (59). There is usually a list showing the star together with the integer SHA and GHA and then the minutes to be applied for each month.

### 6.2 Method B - Polynomial Coefficients

The model contains the data for 1991-2025 on five-year tables. Using the example above, the system looks up the coefficients and calculates the GHA and DEC

| Star GHA and DEC | GHA | DEC |
| :--- | ---: | ---: |
|  | 30.0283000 | -16.4990000 |
| a $_{1}$ | 0.9999605 | 0.0000058 |
| a $_{2}$ | 0.0028000 | -0.0009000 |
| a3 | -0.0052000 | 0.0005000 |
| a4 | 0.0000700 | 0.0000000 |
| Check Sum | 31.0258605 | 16.4986058 |
| L |  | 34.226, |
| Calculated | $64.2503^{\prime}$, | $34.226^{\prime}$ |
| GHA and DEC | $\mathbf{3 2 5 . 0 7 1 2}$ | $\mathbf{1 6 . 4 9 9 1}$ |

The algorithms are similar to the Sun:
Calculate $\mathrm{L}=0.9856474 *(\mathrm{D}+\mathrm{d}+\mathrm{GMT} / 24)$
$\mathrm{D}=$ Number of days from 0:0:0 on $1 / 1 / 91$ or $1 / 1 / 96 . d$ is the day of the month.
For information $\mathrm{GHA}_{\text {(Aries) }}$ can be derived from $98.9513^{\prime}+\mathrm{L}+(15 *$ GMT in decimal hours $)$
The expressions for the GHA and DEC are:

$$
\begin{aligned}
& \text { GHA }=\mathrm{a}_{0}+\left(\mathrm{a}_{1} * \mathrm{~L}\right)+\left(\mathrm{a}_{2} * \sin \mathrm{~L}\right)+\left(\mathrm{a}_{3} * \cos \mathrm{~L}\right)+(15 * \text { GMT in decimal hours }) \\
& \text { DEC }=\mathrm{a}_{0}+\left(\mathrm{a}_{1} * \mathrm{~L}\right)+\left(\mathrm{a}_{2} * \sin \mathrm{~L}\right)+\left(\mathrm{a}_{3} * \cos \mathrm{~L}\right)
\end{aligned}
$$

No semi-diameter is required for stars.

[^3]
### 6.3 Polar Stars

You can use the model to calculate latitude with the polar stars e.g. the latitude of the observer when Polaris (58) is observed at $50^{\prime} 27.82^{\prime \prime}$ at GMT 17:23:17 on 15 January 1997 at longitude $1^{\prime} \mathrm{E} 15{ }^{\prime \prime}{ }^{\prime}$.

The model provides the answer: Latitude $=49.7170^{\prime}\left(49^{\prime} \mathrm{N} 42.57^{\prime \prime}\right)$. Azimuth $=1.250^{\prime}\left(1^{\prime} \mathrm{E} 17.8^{\prime \prime}\right)$.

| DR Position: | , |  |  |  | Calculated Position: |  |  | A | English |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DR Latitude |  | $49^{\prime} \mathrm{N}$ | 43.00 " |  | $50^{\prime} \mathrm{N}$ | 24.79 " |  | Confidence | 0.00\% |
| DR Longitude |  | $1^{\prime} \mathrm{E}$ | 15.00 " |  | $1^{\prime} \mathrm{E}$ | $45.35{ }^{\prime \prime}$ |  | Ellipse |  |
| DR Zone Date |  | 15-Jan-97 | Wednesday |  | Distance | 46.164 mls |  | Latitude | 0.00 mls |
| Zone / GMT |  | 17:23:17 | 17:23 GMT |  | Bearing | 25.90 T |  | LongitudeBearing | 0.00 mls |
| Course / Speed |  | 0.00 T | 0.00 kn |  |  |  |  |  | N/A |
|  | Sight \# 1 |  |  |  | Sight \# 2 |  | Sight \# 3 |  |  |
| Which Sight/Name |  | 2 | Star |  | 2 | Star |  | 0 | N/K |
| Method : 'A' or 'B' |  | B | Polynomial |  | B | Polynomial |  | A | Almanac |
| Actual Sight Time |  | 17:23:17 | 17:23 GMT |  | 17:23:17 | 17:23 GMT |  | 0:00:00 | 00:00 GMT |
| Time Diff. / Miles |  | 0:00 hrs | 0.00 mls |  | 0:00 hrs | 0.00 mls |  | 0:00 hrs | 0.00 mls |
| Revised DR Position |  | $49^{\prime} 43^{\prime \prime} \mathrm{N}$ | $1^{\prime} 15^{\prime \prime} \mathrm{E}$ |  | $49^{\prime} 43^{\prime \prime} \mathrm{N}$ | $1^{\prime} 15^{\prime \prime} \mathrm{E}$ |  | 0 | 0 |
| DR Star Altitude ' | V | 0.00' | 0 |  | 0.00' | 0 |  | 0.00' | 0 |
| DR Star Bearing ' | , | 0.00 E | 0 |  | 0.00 E | 0 |  | 0.00 E | 0 |
| Star Number | V | 58 | Polaris | Input Star No | 10 | Aldebaran |  | 0 | 0 |
| DR Alt. / Bearing | V | $49^{\prime} 42.59^{\prime \prime}$ | $0{ }^{\prime} 24.14{ }^{\prime \prime}$ |  | 36 ' 57.03' | 109 ' 44.49" |  | 0 | $0^{\prime} 0^{\prime \prime}$ |
| Observed Angle Index Error: Minutes |  | $\begin{gathered} 50^{\prime} \\ 0.00^{\prime \prime} \end{gathered}$ | 27.82 " |  | $\begin{gathered} 37^{\prime} \\ 0.00^{\prime \prime} \end{gathered}$ | 2.70 " | $\begin{gathered} 0^{\prime} \\ 0.00^{\prime \prime} \end{gathered}$ |  | 0.00 " |
|  |  |  |  |  |  |  |  |  |  |
| On/Off the Arc: N/F |  | F | Off Arc |  | $\begin{gathered} F \\ 0.00 \mathrm{mtr} \end{gathered}$ | Off Arc | Planet Corr. | F | Off Arc |
| Height of User's Eye |  | 2.00 mtr |  |  |  |  |  | 6.00 mtr |  |
| Enter 'L' |  | L | Lower |  | L Lower |  |  | L | Lower |
| Calc. HP / SD | V | 0.00 " | $0^{\prime \prime}$ | Calc. HP/SD | 0.00 " | $0^{\prime \prime}$ |  | 0.00 " | $0^{\prime \prime}$ |
| Corrected Altitude |  | $50^{\prime} 24.51^{\prime \prime}$ |  | $37^{\prime} 1.38^{\prime \prime}$ |  |  |  | $0^{\prime} 0^{\prime \prime}$ |  |
| Calc. Declination |  | $0^{\prime} \mathrm{N}$ | 0.00 " | Calc. DEC | $0^{\prime} \mathrm{N}$ | 0.00 " | Input DEC | $0^{\prime} \mathrm{N}$ | 0.00 " |
|  |  | $0^{\prime}$ | 0.00 " |  | $0^{\prime}$ | 0.00 " |  | $0^{\prime}$ | 0.00 " |
|  |  | $0^{\prime}$ | 0.00 " |  | 0 ' | 0.00 " |  | $0^{\prime}$ | 0.00 " |
| Star Declination | v | $0^{\prime} 44.7^{\prime \prime}$ | North | Star DEC | $16^{\prime} 30.08^{\prime \prime}$ | North | N/K DEC | $0^{\prime \prime} 0^{\prime \prime}$ | North |
| Calc. GHA |  | $0^{\prime} \mathrm{E}$ | 0.00 " | Calc. GHA | $0^{\prime} \mathrm{E}$ | 0.00 " | Input GHA | $0^{\prime} \mathrm{E}$ | 0.00 " |
|  |  | $0^{\prime}$ | 0.00 " |  | $0^{\prime}$ | 0.00 " |  | $0^{\prime}$ | 0.00 " |
|  |  | $0^{\prime}$ | 0.00 ${ }^{\text {" }}$ |  | $0^{\prime}$ | 0.00 " |  | $0^{\prime}$ | 0.00 " |
| Star GHA / LHA |  | 338' $37.21^{\prime \prime}$ | 339 ' 52.21" | Star LHA | $307{ }^{\prime} 4.55^{\prime \prime}$ | $308^{\prime \prime} 19.55^{\prime \prime}$ | N/K LHA | $0^{\prime \prime} 0^{\prime \prime}$ | $0^{\prime} 0^{\prime \prime}$ |

The model calculates Aries and then GHA and p (polar distance) using polynomial coefficients:

$$
\begin{aligned}
& \mathrm{L}=0.9856474 *(\mathrm{D}+\mathrm{d}+\mathrm{GMT} / 24) \\
& \mathrm{GHA}=\mathrm{a}_{0}+\left(\mathrm{a}_{1} * \mathrm{~L}\right)+\left(\mathrm{a}_{2} * \sin \mathrm{~L}\right)+\left(\mathrm{a}_{3} * \cos \mathrm{~L}\right)+(15 * \text { GMT in decimal hours }) \\
& \mathrm{p}=\mathrm{a}_{0}+\left(\mathrm{a}_{1} * \mathrm{~L}\right)+\left(\mathrm{a}_{2} * \sin \mathrm{~L}\right)+\left(\mathrm{a}_{3} * \cos \mathrm{~L}\right)
\end{aligned}
$$

It calculates the LHA $=(\mathrm{GHA}+$ longitude in hours $) . \mathrm{Ho}=$ Observed Altitude
Latitude $=$ Ho $-(\mathrm{p} * \cos$ LHA $)+0.0087 *(\mathrm{p} * \sin$ LHA $) *(\mathrm{p} * \sin$ LHA $) * \tan$ Ho
Azimuth of Polaris (58) $=0-(\mathrm{p} * \sin$ LHA) $/ \cos$ Ho
Azimuth of Octantis $(59)=180+(\mathrm{p} * \sin$ LHA $) / \cos$ Ho

[^4]

## 7 Star Charts

### 7.1 Star Numbers

Systematic Navigation like The Nautical Almanac uses this list to identify stars by number. The example above uses star Aldebaran (10) which had an SHA of 291' in 1996. This table assumed a date of 1996.


### 7.2 Star Finder

The model allows you three methods of identifying and using stars. The model prompts you in the dialog boxes or you can select stars as one of the options on the End Results box.

Often you have a star sight and need to identify it or alternatively you can check a computed altitude and bearing before using the observation. The options are:

- Star Identification: A box requests the altitude and bearing of a star. Press 'Re-Do' to return to the previous screen or 'OK' to continue. Enter an altitude and bearing and the system calculates the star number and name from the list. Enter the star number and 'OK' to continue or 'Re-Do' to re-enter the altitude and bearing. The model then moves to request the Observed Angle.

Example: Deneb (53) at a bearing of $52^{\prime} \mathrm{E}$ and an altitude of $28.5^{\prime}$ at $32^{\prime} \mathrm{N} 45^{\prime \prime} 15^{\prime} \mathrm{W} 30^{\prime \prime}$ on 9 February 1996 at GMT $07: 03: 52^{6}$. The system performs the mathematics 'backwards' and derives the DEC as 45.3817 ' N and the LHA as 278.6130'. The GHA is therefore 294.2691'.

Star Identification

| Sight (1) |  |  | Sight (2) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bearing | 0.000 | 0.0000 | Bearing | 52.000 | 0.1670 |
| Altitude | 0.000 LHA | 0.0000 E | Altitude | 28.500 LHA | 279.6130 E |
|  | $0.0000^{\prime}$ GHA | 0.0000 E |  | $0.9556^{\prime}$ GHA | 294.2691 E |
| DEC Rads | $0.0000^{\prime}$ Aries | 0.000 | DEC Rads | $0.7921{ }^{\prime}$ Aries | 14644.636 |
| Declination | 0.0000 N Aries | 0.0000 E | Declination | 45.3817 N Aries | 244.6356 E |
|  | SHA | 0.0000 E |  | SHA | 49.6335 E |
|  | Integer | 0 |  | Integer | 49 |
| Satr SHA | Match No | 0 |  | Match No | 53 |
| Star Name | Star | 0 |  | Star | 53 Deneb |

The system calculates GHA(Aries) as $244.6356^{\prime}$ and derives the Sidereal Hour Angle as 49.6335'. It then compares this to the list of SHA's and finds number 53 (Deneb) to be the best match.

- Star Finder: You are prompted to enter the star number on the Star Identification box. The identification is dimmed. Press 'OK' to continue or 'Re-Do' to return to the Options box. The altitude and bearing of the star is calculated using the sight reductions calculations below. The system calculates the altitude at $26.3608^{\prime}$ and the bearing at $52.218^{\prime}$ for Deneb (53) at the sight time and position.

| Altitude | Sight (1) | Sight (2) | Sight (3) |
| :---: | :---: | :---: | :---: |
| Computed Altitude (Hc) Angle in Degrees Azimuth Angle Angle in Degrees Corrected Azimuth (Z) Angle in Degrees Latitude Difference (P) Latitude as Miles Towards / Away | $0.6675^{\prime}$ $38.2463^{\prime}$ $2.2589^{\prime}$ $129^{\prime} 25.4^{\prime \prime}$ $230.5766^{\prime}$ $230^{\prime} 34.6^{\prime \prime}$ $0.0774^{\prime}$ 4.65 mls Towards | $\begin{array}{r} 0.4972^{\prime} \\ 28.4863^{\prime} \\ 0.9099^{\prime} \\ 52^{\prime} 7.92^{\prime \prime} \\ 52.1319^{\prime} \\ 52^{\prime} 7.92^{\prime \prime} \\ 0.1053^{\prime} \\ 6.32 \mathrm{~s}^{2} \end{array}$ Away | $0.3942^{\prime}$ $22.5850^{\prime}$ $2.2058^{\prime}$ $126^{\prime} 23.02^{\prime \prime}$ $126.3836^{\prime}$ $126^{\prime} 23.02^{\prime \prime}$ $0.0388^{\prime}$ 2.33 mls Towards |

The options are then 'OK' to continue, 'Re-Do' to re-enter the Star Options or print preview Stars charts.
An alternative is to click the Stars Chart which print previews a plot of bearings and altitudes at the DR Time. This is an overlay graph with the bearing on the left-hand Y scale and the altitude on the right-hand scale. This can be reviewed in more detail using the magnification within Print Preview or printed for future reference. This option is repeated in the End Options if missed at this stage.

You then have a further option to sort the stars by SHA, bearing or altitude e.g. to check which stars should be visible. Select a sort order and the system sorts the data and print previews the plot.

- Input Star Number: You input the star number and the system does not recalculate.

[^5]These are the two types of star charts available. These use the example above for 9 February 1996 at GMT 12:00:00 at position 32 'N $45^{\prime \prime} 15^{\prime} \mathrm{W} 30$ ".


This second plot is sorted as directed in bearing order to show visible stars


### 7.3 360' Sun, Planets, Moon and Star Chart

There is an option to plot the visible bodies based on altitude on the DegreesCharts sheet. You can plot up to twenty stars and if a star or planet is not visible, N/A will be displayed.

| No | No | Star Name | Mag | C. Altitude | Bearing |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | Sun |  | $39.07{ }^{\prime}$ | 156.01' |
| 2 |  | Venus |  | $26.86{ }^{\prime}$ | 109.44' |
| 3 |  | Mars |  | $37.60^{\prime \prime}$ | 149.45' |
| 4 |  | Jupiter |  | $29.47^{\prime}$ | 206.21 |
| 5 |  | Saturn |  | $28.92^{\prime}$ | 117.73' |
| 6 |  | Moon N/A |  | (21.56') | 277.66' |
| 1 | 53 | 53 Deneb | 1.3 | $76.38^{\prime \prime}$ | $21.20^{\prime}$ |
| 2 | 49 | 49 Vega | 0.1 | $69.55{ }^{\prime}$ | 293.98' |
| 3 | 51 | 51 Altair | 0.9 | $65.53{ }^{\prime}$ | 193.77' |
| 4 | 54 | 54 Enif | 2.5 | $59.03^{\prime}$ | $132.56{ }^{\prime}$ |
| 5 | 47 | 47 Eltanin | 2.4 | 58.89' | 317.29' |
| 6 | 46 | 46 Rasalhague | 2.1 | 48.54' | $250.28^{\prime}$ |
| 7 | 57 | 57 Markab | 2.6 | 47.53' | 103.96' |
| 8 | 1 | 1 Alpheratz | 2.2 | 40.17 | $77.70^{\prime}$ |
| 9 | 3 | 3 Schedar | 2.5 | $39.40^{\prime}$ | 40.97' |
| 10 | 40 | 40 Kochab | 2.2 | 33.89' | $341.07{ }^{\prime}$ |
| 11 | 58 | 58 Polaris | 2.1 | $32.80{ }^{\prime \prime}$ | 0.89' |
| 12 | 41 | 41 Alphecca | 2.3 | $30.22^{\prime \prime}$ | 284.13' |
| 13 | 50 | 50 Nunki | 2.1 | $28.07{ }^{\prime}$ | 199.95' |
| 14 | 44 | 44 Sabik | 2.6 | $24.68{ }^{\prime \prime}$ | $229.46^{\prime}$ |
| 15 | 34 | 34 Alkaid | 1.9 | 20.37 | $316.32^{\prime}$ |
| 16 | N/A | N/A | N/A | N/A | N/A |
| 17 | N/A | N/A | N/A | N/A | N/A |
| 18 | N/A | N/A | N/A | N/A | N/A |
| 19 | N/A | N/A | N/A | N/A | N/A |
| 20 | N/A | N/A | N/A | N/A | N/A |



## 8 Moon

### 8.1 Method A - Aries

Select Method 'A' and no inputs are required. The model uses a complex set of algorithms to derive the GHA, DEC and HP which are outside the scope of this manual ${ }^{7}$. See the second page of the Aries schedule for the workings.

Example: Moon's GHA, DEC and HP on 27 September 1996 at GMT 05:47:22 ${ }^{8}$. This is an extract from the 'Inputs' sheet:

|  | Sight \# 1 |  |  | Sight \# 2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Which Sight |  | 3 | Moon |  | 3 | Moon |
| Method : 'A' or 'B' |  | A | Calculated |  | B | Polynomial |
| Actual Sight Time |  | 5:47:22 | 05:47 GMT |  | 5:47:22 | 05:47 GMT |
| Time Diff. / Miles |  | 0:00 hrs | 0.00 mls |  | 0:00 hrs | 0.00 mls |
| Revised DR Position |  | $0^{\prime \prime} 0{ }^{\prime \prime} \mathrm{S}$ | $0^{\prime} 0^{\prime \prime} \mathrm{W}$ |  | $0^{\prime \prime} 0^{\prime \prime} \mathrm{S}$ | $0^{\circ} 0^{\prime \prime} \mathrm{W}$ |
| DR Star Altitude ' | , | 0.00' | 0 |  | $28.00^{\prime}$ | 0 |
| DR Star Bearing ' |  | 0.00 E | 0 |  | 52.00 E | 0 |
| Star Number |  | 0 | 0 |  | 53 |  |
| DR Alt. / Bearing | , | $2^{\prime} 20.02^{\prime \prime}$ | $272{ }^{\prime} 34.62^{\prime \prime}$ |  | $2^{\prime} 20.42^{\prime \prime}$ | $272{ }^{\prime} 34.18^{\prime \prime}$ |
| Observed Angle | 3 ' |  | 28.00 " | $\begin{gathered} 3^{\prime} \\ 0.00{ }^{\prime \prime} \end{gathered}$ |  | 28.00 " |
| Index Error: Minutes | 0.00 " |  | Off Arc |  |  |  |
| On/Off the Arc: $\mathrm{N} / \mathrm{F}$ |  | F |  | Calc. HP/SD | F | Off Arc |
| Height of User's Eye |  | 6.00 mtr |  |  | 6.00 mtr |  |
| Upper / Lower Limb |  | L | Lower |  | L | Lower |
| Moon HP/SD |  | 0.00 " | 59.7 "/16.3" |  | 0.00 " | 0"/16.3" |
| Corrected Altitude | , | $4^{\prime} 26.24{ }^{\text {" }}$ |  |  | $4^{\prime} 26.33^{\prime \prime}$ |  |
| Calc Moon DEC |  | $0^{\prime} \mathrm{N}$ | 0.00 " | Calc. DEC | $0^{\prime} \mathrm{N}$ | 0.00 " |
|  |  | 0 ' | 0.00 " |  | 0 ' | 0.00 " |
|  | $\checkmark$ | 0 ' | 0.00 " |  | 0 ' | 0.00 " |
| Moon Declination |  | $2^{\prime} 34.49^{\prime \prime}$ | North | Moon DEC | $2^{\prime} 34.05^{\prime \prime}$ | North |
| Calc Moon GHA |  | 0 'E | 0.00 " | Calc. GHA | 0 ' E | 0.00 " |
|  |  | 0 ' | 0.00 " |  | $0{ }^{\prime}$ | 0.00 " |
|  |  | 0 ' | 0.00 " |  | 0 ' | 0.00 " |
| Moon GHA / LHA |  | 87' $39.84{ }^{\prime \prime}$ | $87^{\prime} 39.84{ }^{\prime \prime}$ | Moon LHA | 87' $39.44{ }^{\prime \prime}$ | $87^{\prime} 39.44{ }^{\prime \prime}$ |

### 8.2 Method B - Input Polynomial Coefficients

Chebyshev monthly coefficients are available in the model as in the example above (Sight 2).
The Moon's right ascension (RA) and declination (DEC) are derived from trigonometric expressions involving $\lambda, \beta$ and the adopted value of the obliquity $\varepsilon=23^{\circ} .44$.

The time variable $x$ is calculated from:

$$
x=(d+\mathrm{UT} / 24) / 32
$$

where $d$ is the day of the month and $\mathrm{UT}^{\mathrm{h}}$ is the universal time in hours.
Each of the quantities $\lambda, \beta$ and HP is derived as follows:

$$
\text { Calculate } y=2(2 x-1)
$$

$$
\text { Set } b n+l=b n=0
$$

Use the recurrence relation
$b_{i}=y b_{i}+1-b_{i}+2+a_{i}$ for $i=n-1, n-2, \ldots, 2,1,0$ to calculate $b_{2}$ and $b_{0}$. Then the required quantity, in degrees, is obtained from the expression: $\left(b_{0}-b_{2}+a_{0}\right) / 2$

The Moon's RA and DEC are calculated from $\lambda$ and $\beta$ as follows:

[^6]Set $X=\cos \beta \cos \lambda Y=\cos \varepsilon \cos \beta \sin \lambda-\sin \varepsilon \sin \beta$ and $Z=\sin \varepsilon \cos \beta \sin \lambda+\cos \varepsilon \sin \beta$
where $\varepsilon=23^{\circ} .44$

Then $\mathrm{RA}^{\circ}=\tan -1(Y / X)$ and $\mathrm{DEC}^{\circ}=\sin -1 Z$

If $X<0$ add $180^{\circ}$ to RA. If $X>0$ and $Y<0$ add $360^{\circ}$ to RA.

To obtain the Greenwich hour angle of the Moon (GHA) calculate:
$L^{\circ}=0.9856474\left(D+d+\mathrm{UT}^{\mathrm{h}} / 24\right)$
where UTh is the universal time in hours, $d$ is the day of the month and $D$ is the number of days elapsed as per the table January 0 at $O^{\mathrm{h}}$ UT to the beginning of the month on day 0 at $0^{\mathrm{h}}$ UT. Alternatively it may be calculated using the formula in section 4.2 .

Then GHA Aries $=99^{\circ} .3133+L^{\circ}+15 \mathrm{UT}^{\mathrm{h}}$ and GHA $=$ GHA Aries - RA.

This is a detail from the complex Chebyshev calculations showing the RA, GHA and DEC.
(1) Calculation of Factors

|  | $27-$ Sep-96 |
| :--- | ---: |
|  | $05: 47: 22$ |
| UT | 5.7894 |
| Lookup R | 98.9513 |
| Base Year for D | 1996 |
|  |  |
| D | 244 |
| d | 27 |
| x | 0.851288339 |
| y | 1.405153356 |
| L | 267.34821 |
| Data Line No | 69 |


|  | $\boldsymbol{\lambda}$ | $\boldsymbol{\beta}$ | HP |
| :--- | ---: | ---: | ---: |
|  | 13 | 13 | 8 |
|  | 0 | 0 | 0 |
|  | 0 | 0 | 0 |
|  | 0 | 0 | 0 |
|  | 0.0017 | 0.0026 | 0 |
|  | -0.0065 | 0.0061 | 0 |
|  | -0.0204 | 0.0063 | 0 |
|  | -0.0066 | -0.0025 | 0 |
|  | 0.0984 | -0.0659 | 0 |
|  | 0.1099 | -0.1153 | 0.0025 |
|  | 0.0129 | 0.0599 | 0.0019 |
|  | -0.3676 | 0.9706 | 0.0038 |
|  | -2.5616 | 1.0056 | -0.0052 |
|  | 1.1953 | -3.8168 | -0.0434 |
|  | 5.7793 | -2.1718 | 0.0121 |
|  | 209.9832 | 0.635 | 0.0083 |
|  | 216.4644 | -1.2178 | 0.9549 |
| Sum | 430.6824 | $(4.7040)$ | 0.9349 |

(2) Right Ascension and Declination

| RA/DEC Calculations |  |  |  |
| :--- | ---: | ---: | ---: |
| B15 | 0 | 0 | 0 |
| B14 | 0 | 0 | 0 |
| B13 | 0 | 0 | 0 |
| B12 | 0.0017 | 0.0026 | 0 |
| B11 | -0.004111239 | 0.0097534 | 0 |
| B10 | -0.027876922 | 0.01740502 | 0 |
| B9 | -0.041660111 | 0.01220332 | 0 |
| B8 | 0.067738077 | -0.0661575 | 0 |
| B7 | 0.246742497 | -0.2204647 | 0.0025 |
| B6 | 0.291872971 | -0.1837293 | 0.00541288 |
| B5 | -0.204216212 | 0.93289692 | 0.00890593 |
| B4 | -3.140428067 | 2.50019251 | 0.00190132 |
| B3 | -3.013266827 | -1.236543 | -0.0496343 |
| B2 | 4.685626071 | -6.4095251 | -0.0595451 |
| B1 | 219.58049 | -7.1348227 | -0.0257357 |
| B0 | 520.3230365 | -4.8337949 | 0.97828248 |

(3) Remove Multiples and Calculate GHA, DEC, HP and SD

|  | $\boldsymbol{\lambda}$ | $\boldsymbol{\beta}$ | HP |
| :--- | :--- | :--- | :--- |
| Result | 366.0509052 | 0.17896507 | 0.99636379 |
| Remove Multiples | 6.050905219 | 0.17896507 | 0.99636379 |
|  |  |  |  |
| Radians | 0.105608219 | 0.00312353 | 0.01738983 |


| C Constant | 23.44 |
| :--- | ---: |
| $\varepsilon$ Constant Radians | 0.409105177 |
| X | 0.994423782 |
| Y | 0.095470143 |
| Z | 0.044797247 |
|  |  |
| RA | 0.095712149 |
| Degrees | 5.483902172 |
| X $>180 ?$ | 5.483902172 |
| RA: Remove Multiples | 5.483902172 |
|  |  |


| L | 267.34821 |
| :--- | ---: |
| GHA Aries | 453.1411767 |
| Remove Multiples | 93.14117669 |
| GHA | 87.65727451 |
| GHA: Remove Multiples | 87.65727451 |
| Minutes | 39.43647086 |


| DEC | 0.044812244 |
| :--- | :--- |
| DEC Degrees | 2.567552461 |
| Minutes | 34.05314764 |


| HP | 0.996363793 |
| :--- | :--- |
| Minutes | 59.78182759 |


| SD | 0.271409497 |
| :--- | :--- |
| Minutes | 16.28456983 |

## 9 Planets

### 9.1 Method A - Input GHA and DEC

The GHA and DEC box requests the Greenwich Hour Angle and Declination for GMT 0:0:0 on the day of the sight. Planets also need the correction per hour and this is also found on the daily page in the Almanac. Press 'Re-Do' to re-enter information or 'OK' to continue to the Options Box at the end of the Sight.

Example: The GHA and DEC of Mars on 28 March 1996 at GMT 12:0:0.
From The Nautical Almanac, the GHA and DEC at GMT 0:0:0 is $182^{\prime} 57.3^{\prime \prime}$ and 0 'N $16.6^{\prime \prime}$ respectively. The variations per hour are $15.011458^{\prime}$ and $0.791667^{\prime}$ and the model interpolates the data. Publications such as The Nautical Almanac provide shorter intervals by displaying data in hourly intervals.

The interpolation formula is:
$\mathrm{GHA}_{(\text {day } 0)}$ at GMT 0:0:0 + decimal hours $*\left[\left(\mathrm{GHA}_{(\text {day } 1)}-\mathrm{GHA}_{(\text {day } 0)}\right) / 24\right]$
In this case: $182.966+12 *[(360+(183.230-182.966)) / 24]=182.966+(12 * 15.011458)=363.0925$,
Removing multiples of $360^{\prime}, \mathrm{GHA}=3.0925^{\prime}\left(3^{\prime} 5.5^{\prime \prime}\right)^{9}$

| Mars GHA and DEC | Sight |
| :--- | :--- |
| Mars GHA | $182.955^{\prime}$ |
| Mean Variation | $15.0115^{\prime}$ |
| Correction 12 hours | $180.1374^{\prime}$ |
| Calculated GHA | $273.0237^{\prime}$ |
| Mars GHA | $\mathbf{3 . 0 9 2 5}$ ' $\left.\mathbf{3}^{\prime} \mathbf{5 . 5 4 9}{ }^{\prime}{ }^{\prime}\right)$ |
| Mars DEC | $0.276667^{\prime} \mathrm{N}$ |
| Daily Variation | $0.316663^{\prime}$ |
| Hourly Variation | $0.013194^{\prime}$ |
| Variation 12 hours | $0.158332^{\prime}$ |
| Mars Declination | $\mathbf{0 . 4 3 4 9 9 9 ^ { \prime } ( \mathbf { 0 } \mathbf { N ~ 2 6 . 0 9 9 ` ' ) ~ }}$ |

This is an extract from the 'Inputs' sheet showing both methods. The left hand column shows the results using Method 'A' and the right hand column, Method ' B ' (see next page).


[^7]
### 9.2 Method B - Polynomial Coefficients

The model contains all the coefficients $\mathrm{a}_{0}$ to $\mathrm{a}_{4}$ for GHA and DEC, together with $\mathrm{a}_{0}$ and $\mathrm{a}_{1}$ for the semi-diameter.
The system looks up the coefficients from the relevant schedule. There are separate schedules for Venus, Mars, Jupiter and Saturn providing monthly data for each month from January 1991 to December 2025.

Using the example above, the polynomial coefficients are:

| Mars GHA and DEC | GHA | DEC |
| :---: | :---: | :---: |
| $\mathrm{a}_{0}$ | 11.7031500 | -8.4901000 |
| $\mathrm{a}_{1}$ | 0.5327300 | 9.7093000 |
| a2 | 0.0473400 | 0.6257000 |
| a3 | -0.0140400 | -0.3136000 |
| a4 | 0.0013800 | 0.0052000 |
| Check Sum | 12.2705600 | 1.5365000 |
| Days : X | 0.8906 | 87.230 |
| Calculated | $12.2061{ }^{\prime}$ | $0.4353 '$ |
| GHA and DEC | 363.0917' | 0.4353' |
| Degrees | 3' 5.502'' | $0^{\prime}$ N 26.118' |
| HP a0 | 0.00100 |  |
| HP a 1 | 0.00000 |  |
| Check Sum | 0.00100 |  |
| Horizontal Parallax | $0.0010^{\prime}$ |  |
| HP Minutes | 0.06" |  |

The answers are very similar to the Almanac results above.
The calculations using the coefficients are the same as for the Sun:

$$
\text { Time variable } \mathrm{x}=(\mathrm{d}+\mathrm{GMT} / 24) / 32 .
$$

d is the day in the month and GMT the universal time in hours. (GHA - GMT) in hours and DEC in degrees are derived from this expression:

$$
\mathrm{a}_{0}+\left(\mathrm{a}_{1} * \mathrm{x}\right)+\left(\mathrm{a}_{2} * \mathrm{x}^{2}\right)+\left(\mathrm{a}_{3} * \mathrm{x}^{3}\right)+\left(\mathrm{a}_{4} * \mathrm{x}^{4}\right)
$$

The horizontal parallax is calculated using the expression HP $=\mathrm{a}_{0}+\left(\mathrm{a}_{1} * \mathrm{x}\right)$

## 10 Annual Altitude Table

### 10.1 Method

Select Sun, Stars, Moon etc. and press the button to repopulate the table. This has to recalculate many times and will take about three minutes. The resulting table shows the altitude by day for the selected object:


|  |  | $\begin{gathered} \text { 00:00 UT } \\ 00: 00 \end{gathered}$ | $\begin{gathered} \text { 01:00 UT } \\ \text { 01:00 } \end{gathered}$ | $\begin{gathered} \text { 02:00 UT } \\ \text { 02:00 } \end{gathered}$ | $\begin{gathered} \text { 03:00 UT } \\ \text { 03:00 } \end{gathered}$ | $\begin{gathered} \text { 04:00 UT } \\ 04: 00 \end{gathered}$ | $\begin{gathered} \text { 05:00 UT } \\ 05: 00 \end{gathered}$ | $\begin{gathered} \text { 06:00 UT } \\ 06: 00 \end{gathered}$ | $\begin{gathered} \text { 07:00 UT } \\ 07: 00 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 31-Mar-23 | 38.58 | 29.31 | 20.16 | 11.43 | 3.41 | (3.59) | (9.24) | (13.19) |
| 001 | 1-Jan-23 | 25.81 | 16.83 | 7.81 | (0.89) | (8.91) | (15.84) | (21.22) | (24.60) |
| 002 | 2-Jan-23 | 36.42 | 27.58 | 18.51 | 9.60 | 1.19 | (6.39) | (12.74) | (17.46) |
| 003 | 3-Jan-23 | 46.39 | 37.84 | 28.81 | 19.75 | 11.02 | 2.90 | (4.26) | (10.11) |
| 004 | 4-Jan-23 | 55.37 | 47.43 | 38.59 | 29.48 | 20.49 | 11.93 | 4.08 | (2.74) |
| 005 | 5-Jan-23 | 62.58 | 55.94 | 47.62 | 38.62 | 29.48 | 20.56 | 12.13 | 4.47 |
| 006 | 6-Jan-23 | 66.51 | 62.53 | 55.44 | 46.89 | 37.79 | 28.63 | 19.73 | 11.38 |
| 007 | 7-Jan-23 | 65.67 | 65.70 | 61.14 | 53.77 | 45.09 | 35.92 | 26.73 | 17.82 |
| 008 | 8-Jan-23 | 60.52 | 64.25 | 63.42 | 58.40 | 50.84 | 42.08 | 32.86 | 23.62 |
| 009 | 9-Jan-23 | 52.86 | 58.87 | 61.51 | 59.79 | 54.35 | 46.66 | 37.84 | 28.58 |
| 010 | 10-Jan-23 | 43.91 | 51.16 | 56.12 | 57.55 | 54.96 | 49.14 | 41.32 | 32.45 |
| 011 | 11-Jan-23 | 34.27 | 42.22 | 48.57 | 52.30 | 52.51 | 49.12 | 42.95 | 35.01 |
| 012 | 12-Jan-23 | 24.19 | 32.56 | 39.77 | 45.04 | 47.50 | 46.60 | 42.53 | 36.04 |
| 013 | 13-Jan-23 | 13.79 | 22.43 | 30.21 | 36.52 | 40.65 | 41.91 | 40.07 | 35.45 |
| 014 | 14-Jan-23 | 3.09 | 11.91 | 20.09 | 27.16 | 32.51 | 35.54 | 35.80 | 33.22 |
| 015 | 15-Jan-23 | (7.90) | 1.05 | 9.54 | 17.17 | 23.47 | 27.91 | 30.01 | 29.49 |
| 016 | 16-Jan-23 | (19.15) | (10.13) | (1.40) | 6.68 | 13.75 | 19.35 | 23.04 | 24.44 |
| 017 | 17-Jan-23 | (30.60) | (21.58) | (12.67) | (4.20) | 3.51 | 10.09 | 15.15 | 18.32 |
| 018 | 18-Jan-23 | (42.05) | (33.15) | (24.13) | (15.34) | (7.08) | 0.35 | 6.62 | 11.39 |
| 019 | 19-Jan-23 | (52.96) | (44.49) | (35.51) | (26.49) | (17.76) | (9.59) | (2.26) | 3.93 |
| 020 | 20-Jan-23 | (61.95) | (54.75) | (46.23) | (37.21) | (28.16) | (19.38) | (11.14) | (3.71) |
| 021 | 21-Jan-23 | (65.95) | (62.06) | (55.10) | (46.66) | (37.63) | (28.49) | (19.57) | (11.13) |
| 022 | 22-Jan-23 | (62.28) | (63.33) | (59.96) | (53.43) | (45.20) | (36.20) | (26.97) | (17.87) |
| 023 | 23-Jan-23 | (53.14) | (57.77) | (58.74) | (55.70) | (49.58) | (41.61) | (32.71) | (23.44) |
| 024 | 24-Jan-23 | (41.72) | (48.19) | (52.19) | (52.79) | (49.79) | (43.92) | (36.19) | (27.41) |
| 025 | 25-Jan-23 | (29.60) | (37.05) | (42.80) | (46.01) | (46.05) | (42.88) | (37.09) | (29.52) |
| 026 | 26-Jan-23 | (17.44) | (25.47) | (32.27) | (37.20) | (39.58) | (39.01) | (35.56) | (29.75) |
| 027 | 27-Jan-23 | (5.53) | (13.95) | (21.46) | (27.55) | (31.63) | (33.22) | (32.06) | (28.31) |
| 028 | 28-Jan-23 | 5.98 | (2.72) | (10.74) | (17.66) | (23.02) | (26.32) | (27.20) | (25.54) |
| 029 | 29-Jan-23 | 17.04 | 8.13 | (0.28) | (7.86) | (14.20) | (18.89) | (21.51) | (21.81) |
| 030 | 30-Jan-23 | 27.60 | 18.55 | 9.82 | 1.71 | (5.44) | (11.25) | (15.37) | (17.44) |
| 031 | 31-Jan-23 | 37.58 | 28.48 | 19.50 | 10.95 | 3.13 | (3.65) | (9.04) | (12.71) |
| 032 | 1-Feb-23 | 46.82 | 37.81 | 28.68 | 19.78 | 11.38 | 3.78 | (2.72) | (7.80) |
| 033 | 2-Feb-23 | 54.91 | 46.31 | 37.21 | 28.07 | 19.21 | 10.92 | 3.46 | (2.86) |
| 034 | 3-Feb-23 | 61.06 | 53.54 | 44.79 | 35.62 | 26.45 | 17.61 | 9.35 | 1.96 |
| 035 | 4-Feb-23 | 63.96 | 58.67 | 50.95 | 42.12 | 32.90 | 23.69 | 14.81 | 6.55 |
| 036 | 5-Feb-23 | 62.60 | 60.64 | 54.97 | 47.12 | 38.24 | 28.96 | 19.71 | 10.78 |
| 037 | 6-Feb-23 | 57.50 | 58.83 | 56.06 | 50.05 | 42.10 | 33.17 | 23.85 | 14.55 |
| 038 | 7-Feb-23 | 50.03 | 53.79 | 53.94 | 50.41 | 44.08 | 36.03 | 27.07 | 17.71 |
| 039 | 8-Feb-23 | 41.25 | 46.60 | 49.08 | 48.12 | 43.93 | 37.32 | 29.17 | 20.17 |

This is a chart for a selected day in the year. Use the combo box to select a specific day in the year.


## Moon phases



## 11 Corrected Altitude

### 11.1 Method

All sextant angles (Hs) need to be corrected for index error and altitude to produce the Apparent Altitude (H). The model computes these adjustments automatically and calculates the Observed Altitude (Ho) by subtracting a correction for refraction. For the Sun, Moon, Venus and Mars a correction for parallax is also applied to H and for the Sun and Moon a further correction for semi-diameter is also required.

The detailed calculations are:

1. dip: $\mathrm{D}=0.0293$ * SQRT h (where h is the height of the eye above the horizon in metres).
2. I is the instrument or index error.
3. Apparent Altitude $\mathrm{H}=\mathrm{Hs}+\mathrm{I}-\mathrm{D}$.
4. Refraction $(\mathrm{R})=0.0167 /(\tan (\mathrm{H}+7.32) /(\mathrm{H}+4.32))$. Alternative $(\mathrm{R})=0.0162 / \tan \mathrm{H}$. An alternative formula is $\mathrm{R}=0.0162 / \tan \mathrm{H}$
5. $\mathrm{f}=0.28 *$ Pressure $/($ Temperature +273$)$.

Adjusted Refraction (Ro) $=\mathrm{f} * \mathrm{R}$.
6. Calculate the parallax in altitude (PA) from the horizontal parallax (HP) and the apparent altitude (H) for the Sun, Moon Venus and Mars PA $=\mathrm{HP} * \cos \mathrm{H}$.

Sun HP $=0.0024^{\prime}$. Moon HP is calculated.
7. Oblateness of the Moon. $\mathrm{OB}=$ minus $0.0017 * \cos \mathrm{H}$.
8. Semi-diameter for the Sun and Moon. Moon $S=0.2724$ ' * HP. Sun $S$ is 16 ' under Method 'A' and computed under Method 'B'. Add lower limb and subtract upper limb.
9. Calculate the Observed Altitude (Ho).

$$
\mathrm{Ho}=\mathrm{H}-\mathrm{R}+\mathrm{PA}+\mathrm{OB} \pm \mathrm{S} .
$$

The model uses the Observed Altitude (Ho) in sight reduction and compares it against the Computed Altitude (Hc) to derive the intercept and azimuth.

This is an extract from the 'Inputs' sheet showing workings for the Moon on 9 February 1996 observed at an altitude of 37 ' 28.02" (37.4167’) ${ }^{10}$.
(C) Corrected Altitude (Decimals)

| Altitude | Sight (1) |  |
| :---: | :---: | :---: |
| Observed (Hs) |  | $37.4167^{\prime}$ |
| Index Error (l) | 0.0000 ${ }^{\prime}$ |  |
| DIP - Height ( $\mathrm{D}=0.0293^{*}$ Sqrth $)$ | -0.0718" |  |
| Apparent Altitude (H=Hs+1-D) |  | 37.3449' |
| $\mathrm{Ro}=0.0167 / \tan (\mathrm{H}+7.31) /(\mathrm{h}+4.4)$ ) | $0.0217^{\prime}$ |  |
| $\mathrm{f}=0.28{ }^{\text {P }}$ Pressure* $^{\text {( }}$ (Temp+273) | $1.000{ }^{\prime}$ |  |
| Refraction (R=Ro*f) |  | $0.0217^{\prime}$ |
| Oblateness of Earth (OB) |  | -0.0014' |
| Parallax (HP) | 0.9386 ${ }^{\prime}$ |  |
| Parallax Altitude (PA=HP** $\cosh$ ) |  | 0.7462' |
| Semi Diameter (S) <br> Corr. Altitude ( $\mathrm{Ho}=\mathrm{H}-\mathrm{R}+\mathrm{PA}+\mathrm{S}$ ) |  | $\begin{array}{r} 0.2558^{\prime \prime} \\ 38.3238^{\prime \prime} \end{array}$ |

[^8]
### 11.2 Observed Angle

This example from The Nautical Almanac $1996^{11}$ assumes a height of 5.4 metres, temperature of $-3.0^{\prime}$ C, pressure of 982 Mb . The date is 22 October 1996 at GMT 10:0:0.

| Altitude | Sun |  | Moon |  | Venus |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Observed (Hs) |  | $21.3283 '$ |  | $33.4600{ }^{\prime}$ |  | 4.5433' |
| Index Error (I) | $0.0000{ }^{\prime}$ |  | 0.0000' |  | 0.0000' |  |
| DIP - Height ( $\mathrm{D}=0.0293 *$ Sqrt H) ${ }^{12}$ | -0.0681" |  | -0.0681" |  | -0.0681" |  |
| Apparent Altitude (H= Hs + I-D) |  | 21.2602' |  | 33.3919' |  | 4.4752' |
| Ro $=0.0167 / \tan [H+7.31 /(h+4.4)]^{13}$ | $0.0423{ }^{\prime}$ |  | 0.0251 ${ }^{\prime}$ |  | 0.1801' |  |
| $\mathrm{f}=0.28$ * Pressure * (Temp + 273) | $1.0184^{\prime}$ |  | 1.0184' |  | 1.0184' |  |
| Refraction ( $\mathrm{R}=\mathrm{Ro}$ * f ) |  | $0.0431{ }^{\prime}$ |  | $0.0256{ }^{\prime}$ |  | 0.1834 |
| Oblateness ( $\mathrm{OB}=-0.0017 * \cos \mathrm{H}$ ) ) |  | $0.0000{ }^{\prime}$ |  | -0.0014' |  | 0.0000' |
| Horizontal Parallax (HP) | 0.0024 |  | 0.9922' |  | 0.0021' |  |
| Parallax in Altitude ( $\mathrm{PA}=\mathrm{HP} * \cos \mathrm{H}$ ) |  | 0.0022' |  | 0.8284' |  | 0.0021' |
| Semi Diameter (S) - add lower limb ${ }^{14}$ |  | $0.2684{ }^{\prime}$ |  | $0.2704{ }^{\prime}$ |  | 0.0000' |
| Corr. Altitude ( $\mathrm{Ho}=\mathbf{H}-\mathrm{R}+\mathrm{PA}+\mathrm{OB} \pm \mathrm{S}$ ) |  | 21.4878 ${ }^{\prime}$ |  | $34.4637{ }^{\prime}$ |  | $4.2940{ }^{\prime}$ |



[^9]
## 12 Sight Reduction

### 12.1 Method

The model uses the classic Marcq Saint Hilaire method to reduce the sights as the mathematical link between the observer and the celestial body. If you know your latitude and longitude, you can predict the true bearing and the height of the object above the horizon. This angle can then be compared to your corrected sextant angle to produce a position line and a measure of distance along this line. With several sights, the model plots a fix through the statistical intersection of these position lines.


The following sight reduction formulae are used:
(1) Computed Altitude (Hc):

$$
\mathrm{Hc}=\mathrm{A} \sin [(\sin \text { Latitude } * \sin \text { Declination })+(\cos \text { Latitude } * \cos \text { Declination } * \cos \text { LHA })]
$$

(2) Azimuth or True Bearing (Z):

$$
\mathrm{Z}=\mathrm{A} \cos [(\sin \text { Declination }-(\sin \text { Computed Altitude } * \sin \text { Latitude })) /(\cos \mathrm{Hc} * \cos \text { Latitude })]
$$

If the Local Hour Angle is less than 180' then the Azimuth is $360^{\prime}$ less the product of the above expression.
This is an extract from the 'Inputs' sheet showing the workings for the example in the previous section:
(D) Sight Reduction

| Altitude | Sight (1) | Sight (2) | Sight (3) |
| :---: | :---: | :---: | :---: |
| Computed Altitude (Hc) | $0.6675^{\prime}$ | 0.4972' | 0.3942' |
| Angle in Degrees | 38.2463' | $28.4863^{\prime}$ | $22.5850^{\prime}$ |
| Azimuth Angle | 2.2589' | 0.9099' | $2.2058^{\prime}$ |
| Angle in Degrees | 129 ' 25.4 " | $52^{\prime \prime} 7.92^{\prime \prime}$ | $126^{\prime} 23.02^{\prime \prime}$ |
| Corrected Azimuth (Z) | $230.5766^{\prime}$ | $52.1319^{\prime}$ | 126.3836' |
| Angle in Degrees | 230 , 34.6 " | $52^{\prime \prime} 7.92^{\prime \prime}$ | 126 ' $23.02{ }^{\prime \prime}$ |
| Latitude Difference (P) | $0.0774^{\prime}$ | $0.1053^{\prime}$ | $0.0388^{\prime \prime}$ |
| Latitude as Miles | 4.65 mls | 6.32 mls | 2.33 mls |

## 13 Calculated Position

### 13.1 Method

An estimate can be made of the position at the adopted time of fix. The position at the time of the observations can then be easily calculated provided that the course and speed has been constant. Using speed (V) in knots and the track (T) the algorithms are:

$$
\begin{aligned}
& \text { Longitude }=\mathrm{L}_{(\mathrm{Fix})}+\mathrm{t}(\mathrm{~V} / 60) * \sin \mathrm{~T} / \cos \mathrm{B}_{\mathrm{F}} \\
& \text { Latitude }=\mathrm{B}_{(\mathrm{Fix})}+\mathrm{t}(\mathrm{~V} / 60) * \cos \mathrm{~T}
\end{aligned}
$$

$\mathrm{L}_{(\mathrm{Fix})}$ and $\mathrm{B}_{(\mathrm{Fix})}$ are the estimated longitude and latitude at the time of fix and ' t ' is the time interval (hours).
Example: $\mathrm{DR}=32^{\prime} \mathrm{N} 45^{\prime \prime}\left(32.75^{\prime} \mathrm{N}\right), 15^{\prime} \mathrm{W} 30^{\prime \prime}\left(15.50^{\prime} \mathrm{W}\right)$ at GMT 12:0:0. A vessel has been on a course of $315^{\prime} \mathrm{T}$ at 12 knots since GMT 6:58:52 ${ }^{15}$. To calculate the start position:

$$
\begin{aligned}
& \text { Longitude }=-15.50+-5.0188 *(12 / 60) * \sin 315^{\prime} / \cos 32.75^{\prime} \\
& \text { Longitude }=-15.50+-5.0188 * 0.20 * 0.70711 / 0.841039=14.6561^{\prime} \mathrm{W} \\
& \text { Latitude }=32.75+-5.0188 *(12 / 60) * \cos 315^{\prime} \\
& \text { Longitude }=32.75+-5.0188 * 0.20 * 0.707107=32.0402^{\prime} \mathrm{N}
\end{aligned}
$$

The position lines for one or more observations can be plotted using the azimuth Z and the intercept p :

$$
\mathrm{p}=\mathrm{Ho}-\mathrm{Hc}
$$

If p is positive the position line is drawn along the azimuth. If p is negative, the position line is away from the assumed position by adding 180 ' to the azimuth. Provided that there are no observation errors, the observer should be close to or along the position line. Two or more position lines are required to determine a fix.

The model uses the 'Method of Least Squares' to determine a fix from up to three observations. $\mathrm{p}_{1}$ and $\mathrm{Z}_{1}$ are the intercept and azimuth for the first observation etc. The model calculates these values:

```
A}=(\mp@subsup{\operatorname{cos}}{}{2}*\mp@subsup{Z}{1}{})+(\mp@subsup{\operatorname{cos}}{}{2}*\mp@subsup{Z}{2}{})+
B}=(\operatorname{cos}\mp@subsup{Z}{1}{}*\operatorname{cos}\mp@subsup{Z}{1}{})+(\operatorname{cos}\mp@subsup{Z}{2}{}*\operatorname{cos}\mp@subsup{Z}{2}{})+
C=( sin}2*\mp@subsup{Z}{1}{})+(\mp@subsup{\operatorname{sin}}{2}{*}*\mp@subsup{Z}{}{2})+
D = (p}\mp@subsup{p}{1}{*}\operatorname{cos}\mp@subsup{Z}{1}{})+(\mp@subsup{p}{2}{}*\operatorname{cos}\mp@subsup{Z}{2}{})+
E=(\mp@subsup{p}{1}{}*\operatorname{sin}\mp@subsup{Z}{1}{})+(\mp@subsup{p}{2}{}*\operatorname{sin}\mp@subsup{Z}{2}{})+\ldots
F}=\mp@subsup{p}{}{2}\mp@subsup{}{1}{}+\mp@subsup{p}{}{2}\mp@subsup{2}{2}{}+
G=A*C-B
```

An improved estimate of the fix is given by:

$$
\begin{aligned}
& \text { Longitude } \mathrm{L}_{\mathrm{I}}=(\mathrm{A} * \mathrm{E}-\mathrm{B} * \mathrm{D}) /\left(\mathrm{G} * \cos \mathrm{~B}_{(\mathrm{fix})}\right) \\
& \text { Latitude } \mathrm{B}_{\mathrm{I}}=(\mathrm{C} * \mathrm{D}-\mathrm{B} * \mathrm{E}) / \mathrm{G} \\
& \text { Departure longitude } \mathrm{dL}=\mathrm{L}_{(\mathrm{fix})}+\mathrm{L}_{\mathrm{I}} \\
& \text { Departure latitude } \mathrm{dB}=\mathrm{B}_{(\mathrm{fix})}+\mathrm{B}_{\mathrm{I}}
\end{aligned}
$$

The model substitutes the DR position with the calculated fix in order to converge on a solution. i.e. $\mathrm{L}_{\mathrm{I}}=\mathrm{L}_{\text {(fix) }}$
The model computes the distance between the assumed position and the improved estimated position in nautical miles from:

$$
\mathrm{d}=60 * \operatorname{SQRT}\left[\left(\mathrm{~L}_{\mathrm{I}}+\mathrm{L}_{(\mathrm{fix})}\right)^{2} * \cos ^{2} * \mathrm{~B}_{(\mathrm{fix})}+\left(\mathrm{B}_{\mathrm{I}}+\mathrm{B}_{\mathrm{fix})}\right)^{2}\right]
$$

[^10]The model iterates the result until it converges on an improved estimate. The number of recalculations is set to 5 and you can always recalculate the model by pressing F9 or the 'Calculate' button.

The system also estimates the error in position. n is the number of observations. The standard deviation of the estimated position in nautical miles is given by:

$$
\text { Standard deviation } \sigma=60 * \operatorname{SQRT}(\mathrm{~S} /(\mathrm{n}-2))
$$

$$
\mathrm{S}=\mathrm{F}-\mathrm{D} * \mathrm{~dB}-\mathrm{E} * \mathrm{dL} * \cos \mathrm{~B}_{\mathrm{F}}
$$

The standard deviations for longitude $\sigma_{\mathrm{L}}$ and latitude $\sigma_{\mathrm{B}}$ are given by:

$$
\sigma_{\mathrm{L}}=\sigma * \operatorname{SQRT}(\mathrm{~A} / \mathrm{G}): \sigma_{\mathrm{B}}=\sigma * \operatorname{SQRT}(\mathrm{C} / \mathrm{G})
$$

The model assumes a probability of 0.95 and computes the size of a confidence ellipse which means that there is a $95 \%$ probability of the revised estimated position lying within the ellipse.

The estimated position has a probability P of being located within a confidence ellipse specified by the axes a and b and the azimuth $\theta$ of the a-axis where:

$$
\begin{aligned}
& \tan 2 * \theta=2 * \mathrm{~B} /(\mathrm{A}-\mathrm{C}) \\
& \mathrm{a}=\sigma * \mathrm{k} / \operatorname{SQRT}(\mathrm{n} / 2+\mathrm{B} / \sin 2 * \theta) \\
& \mathrm{b}=\sigma * \mathrm{k} / \operatorname{SQRT}(\mathrm{n} / 2-\mathrm{B} / \sin 2 * \theta) \\
& \mathrm{k}=\operatorname{SQRT}\left[-2 * \log _{e} *(1-\mathrm{P})\right]=2.448 \text { at a probability of } 95 \%
\end{aligned}
$$

### 13.2 Example

This example applies the theory from the previous sections to bring together the calculation of GHA, LHA, Declination with sight reduction and statistical fixes. This example is taken from Compact Data.

On February 9, 1996 at GMT 12:0:0 the DR position is assumed to be $32^{\prime} \mathrm{N} 45^{\prime \prime} 15^{\prime} \mathrm{W} 30$ ". Three sights have been taken along a course of $315^{\prime} \mathrm{T}$ at a speed of 12 knots. The temperature is $9.8^{\prime} \mathrm{C}$ and the atmospheric pressure 1010 Mb . The height of the eye above the horizon is 6.0 metres. Sextant index error is assumed to $0{ }^{\prime \prime 16}$.

|  | Moon | Star (Deneb 53) | Sun |
| :--- | :---: | :---: | :---: |
|  |  |  |  |
| Time of Sight (GMT) | $6: 58: 52$ | $7: 03: 52$ | $9: 53: 45$ |
| Difference to DR Time | $(5.01 \mathrm{~h})$ | $(4.56 \mathrm{~h})$ | $(2.06 \mathrm{~h})$ |
|  |  |  |  |
| Observed Angle (Hs) | $37^{\prime} 25^{\prime \prime}$ | $28^{\prime} 29^{\prime \prime}$ | $22^{\prime} 28^{\prime \prime}$ |
| Adjusted Altitude (Ho) | $38^{\prime} 19.43^{\prime \prime}$ | $28^{\prime} 22.8^{\prime \prime}$ | $22^{\prime} 37.3^{\prime \prime}$ |
|  |  |  |  |
| Declination | $5^{\prime} 24.85^{\prime \prime} \mathrm{S}$ | $45^{\prime} 16.03^{\prime} \mathrm{N}$ | $14^{\prime} 50.27^{\prime \prime} \mathrm{S}$ |
| GHA | $52^{\prime} 12.08^{\prime \prime}$ | $294^{\prime} 18.94^{\prime \prime}$ | $324^{\prime} 53.11^{\prime \prime}$ |
| LHA | $37^{\prime} 30.48^{\prime \prime}$ | $279^{\prime} 36.5^{\prime \prime}$ | $309^{\prime} 42.14^{\prime \prime}$ |
|  |  |  |  |
| Azimuth / Bearing | $230^{\prime} 36.38^{\prime \prime}$ | $52^{\prime} 4.62^{\prime \prime}$ | $126^{\prime} 19.23^{\prime \prime}$ |
| Intercept / Distance | 0.88 Miles | 0.89 Miles | 0.02 Miles |
| Direction | Away | Away | Towards |

[^11](E) Computed Position

| Position | Sight (1) |  |  | Sight (2) |  | Sight (3) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Azimuth 1 | $410.606^{\prime}$ | -1 | $50.606^{\prime}$ |  |  |  |  |
| Course | 315.00 T |  |  |  |  |  |  |
| Distance2 | $1.0038{ }^{\prime}$ |  |  |  |  |  |  |
| U=90+G | $140.606^{\prime}$ |  |  |  |  |  |  |
| Take out Excess 360 | 140.606' | $140.606^{\prime}$ |  |  |  |  |  |
| U | -0.098 | -0.098' |  |  |  |  |  |
| W+U | -0.083' | $0.083^{\prime}$ |  |  |  |  |  |
| Take out Excess 360 | 230.606 | 230.606 ${ }^{\prime}$ |  |  |  |  |  |
| Latitude | 32.593 N | 32 N | 35.59 " |  |  |  |  |
| Longitude | 15.489 W | 15 W | -29.37 " |  |  |  |  |
| True Azimuth Bearing ( $Z$ ) | 050.606 T | 0.89 mls |  | 232.077 T | 0.89 mls | 126.321 T | 0.02 mls |
| Plot Position / Direction | 039.39 T | NE |  | 037.92 T | SW | 036.32 T | SE |
| Distance | 0.68 mls | 0.56 mls |  | -0.70 mls | -0.55 mls | 0.02 mls | -0.01 ms |
| Bearing Miles | 0.684 E | 0.562 N |  | 0.703 W | 0.548 S | 0.019 E | 0.014 S |
| Latitude/Longitude | 0.013 E | 0.009 E |  | 0.013 W | 0.009 S | 0.000 E | 0.000 S |
| Revised Fix Position | 14.680 W | 31.942 N |  | 14.721 W | 31.936 N | 15.182 W | 32.345 N |
| Minutes | 40.8226 | 56.5454 |  | 43.2376 | 56.1873 | 10.9464 | 20.7249 |

(F) Fix : Method of Least Squares


The Model uses the 'Method of Least Squares' to compute a fix at the DR Time of 32'N 38.59' $15^{\prime} \mathrm{W} 32.17$. This position is on a bearing of 199.45 'T 6.66 miles from the DR Position. The confidence ellipse is $\mathrm{a}=3.27$ nautical miles, $\mathrm{b}=2.11$ nautical miles and the azimuth $\theta$ is $333.25^{\prime}$.


| DR Position: |  |  |  | Calculated Position: |  | Position Error: |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DR Latitude |  | $32^{\prime} \mathrm{N}$ | $45.00^{\prime \prime}$ | $32^{\prime} \mathrm{N}$ | $38.59^{\prime \prime}$ | Confidence |  |
| DR Longitude | , | $15^{\prime} \mathrm{W}$ | -30.00" | $15^{\prime} \mathrm{W}$ | 32.17" | Ellipse | 95.00\% |
| DR Zone Date |  | 9-Feb-96 | Friday |  |  |  |  |
| Zone / GMT |  | 11:00:00 | 12:00 GMT | Distance | Bearing | Latitude | 2.11 mls |
| Course / Speed |  | 315.00 T | 12.00 kn | 6.66 mls | 196.55 T | Longitude | 3.28 mls |
| Temperature \& Pressure |  | $9.80{ }^{\text {C }}$ | 1010.00 mb |  |  | Bearing | 333.25 T |
| Sight \# 1 |  |  |  | Sight \# 2 |  | Sight \# 3 |  |
| Which Sight | 3 Moon A Calculated |  |  | 2 Star <br> B Polynomial |  |  |  |
| Calc/Almanac/Polynomial |  |  |  | A Calculated |
| Star Number |  | 49 |  |  |  | 53 Deneb |  | 0 |  |
| Actual Sight Time |  | 5:58:52 | 06:58 GMT | 6:03:52 | 07:03 GMT | 8:53:45 | 09:53 GMT |
| Time Diff. / Miles |  | 5:01 hrs | 60.23 mls | 4:56 hrs | 59.23 mls | 2:06 hrs | 25.25 mls |
| Revised DR Position |  | $31^{\prime \prime} 56^{\prime \prime} \mathrm{N}$ | $14^{\prime} 41.6^{\prime \prime} \mathrm{W}$ | $31^{\prime} 56.7^{\prime \prime} \mathrm{N}$ | $14^{\prime} 42.4{ }^{\text {" }} \mathrm{W}$ | $32^{\prime} 20.7^{\prime \prime} \mathrm{N}$ | $15^{\prime} 11^{\prime \prime} \mathrm{W}$ |
| DR Alt. / Bearing |  | $38^{\prime}$ 20.31" | 230 ' $36.38{ }^{\prime \prime}$ | $28^{\prime} 23.75{ }^{\prime \prime}$ | $52^{\prime} 4.62^{\prime \prime}$ | $22 \cdot 37.41$ | 126 '19.23" |
| Observed Angle |  | 37' $25.002^{\prime \prime}$ |  | $28^{\prime \prime} 28.998^{\prime \prime}$ |  | $22^{\prime \prime} 28.002^{\prime \prime}$ |  |
| Index Error: Minutes |  | $0.00{ }^{\prime \prime}$ |  | $0.00{ }^{\prime \prime}$ |  | 0.00' |  |
| Height of User's Eye / DIP |  | -4.31" |  | -4.31" |  | -4.31" |  |
| Refraction ( $\mathrm{R}=\mathrm{Ro} 0^{\star} \mathrm{f}$ ) |  | $1.22^{\prime \prime}$ |  | 1.84" |  | $2.40^{\prime \prime}$ |  |
| Parallax in Altitude |  | 44.77" |  | $0.00{ }^{\prime \prime}$ |  | 0.13" |  |
| Semi-Diameter |  | 15.35" |  | $0.00^{\prime \prime}$ |  | 16.00" |  |
| Corrected Altitude |  | 38'19.43" |  | $28^{\prime} 22.86^{\prime \prime}$ |  | $22^{\prime} 37.43^{\prime \prime}$ |  |
| Calc Moon DEC |  | -5' $24.85^{\prime \prime}$ | South | $45^{\prime} 16.03^{\prime \prime}$ | North | -14'50.27" | South |
| Moon GHA / LHA |  | $52^{\prime \prime} 12.07^{\prime \prime}$ | $37^{\prime} 30.48^{\prime \prime}$ | 294' 18.94" | 279 ' $36.5^{\prime \prime}$ | 324' 53.11" | $309^{\prime} 42.14{ }^{\prime \prime}$ |
| Azimuth / Bearing |  | 230'36.38' | 50'36.38' | $52^{\prime} 4.62^{\prime \prime}$ | 232' $4.62^{\prime \prime}$ | 126' $19.23^{\prime \prime}$ | 126' 19.23' |
| Intercept : Miles |  | 0.89 mls | Away | 0.89 mls | Away | 0.02 mls | Towards |
| Calc. Position |  | $31^{\prime} 56.5^{\prime \prime} \mathrm{N}$ | $14^{\prime} 40.8{ }^{\prime} \mathrm{W}$ | $31^{\prime} 56.2^{\prime \prime} \mathrm{N}$ | $14^{\prime} 43.2^{\prime \prime} \mathrm{W}$ | $32^{\prime} 20.7^{\prime \prime} \mathrm{N}$ | $15^{\prime \prime} 10.9{ }^{\prime \prime} \mathrm{W}$ |



## 14 Sun and Moon Rise and Set

### 14.1 Description

The model calculates Sun rise and set for the dead reckoning date and position. Set the application to manual and access the RiseSet schedule after entering assumed position data on the Inputs schedule. Press F9 to recalculate the application as this schedule can require more iterations to converge on the results. It uses these expressions:

```
Calculate t where cost = sin h - (sin Lat * sin Dec}6)/(\operatorname{cos Lat * cos Dec}6
h = -0.8333' for Sun rise or set, - }\mp@subsup{6}{}{\prime}\mathrm{ 'for civil twilight and -12' for nautical twilight.
Sunrise = (90' - Longitude - t - GHA6) / 15
Sunset =(270' - Longitude - t - GHA 18) / 15
```

The model uses similar expressions for the Moon however the passage of this body is more complicated. The system iterates an answer despite the possibility of rising and setting on different days.

The model also derives Sun transits.

## $\mathrm{T}_{1}=12$ - Longitude converted to hours

Time $=24$ - Longitude in hours $-\mathrm{y}_{1}$ where $\mathrm{y}_{1}$ is $($ GHA-GMT $)$ in hours evaluated at time $\mathrm{T}_{1}$
Phases of the Moon


### 14.2 Example

This example is for March 31, 2023 at $50^{\prime} \mathrm{N} 35.14^{\prime \prime} 4^{\prime} \mathrm{W} 55.09{ }^{\prime \prime}$

|  |  | Rise |  |  | Set | Rise and Set Position Data |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Zonetime | GMT/UT | Zonetime | GMT/UT | Azimuth | Declination | GHA | LHA |
| 1 | Sun |  | 05:38 AM | 05:58:16 | 06:30 PM | 18:50:32 | 82' $36.2^{\prime \prime}$ | $4^{4} 4.32{ }^{\prime \prime} \mathrm{N}$ | 268' $29.21{ }^{\prime \prime}$ | 263' $34.12^{\prime \prime}$ |
|  |  |  |  |  |  |  | $277^{\prime} 23.8^{\prime \prime}$ | $4^{\prime} 16.74{ }^{\prime \prime} \mathrm{N}$ | 101'35.59" | 96' $40.5{ }^{\prime \prime}$ |
| 2 | Sun Transit |  | 12:04 PM | 12:23:55 | - | - | $180^{\prime} 0^{\prime \prime}$ | $4^{\prime} 10.32^{\prime \prime} \mathrm{N}$ | $358^{\prime} 56.36^{\prime \prime}$ | $354^{\prime} 1.27^{\prime \prime}$ |
| 3 | Civilian |  | 05:00 AM | 05:19:41 | 07:09 PM | 19:29:09 | $75^{\prime} 4.11$ | $4^{\prime} 3.66{ }^{\prime \prime} \mathrm{N}$ | 258' $50.45^{\prime \prime}$ | 253' $55.36^{\prime \prime}$ |
|  |  |  |  |  |  |  | 284' 55.89 | $4^{1} 17.4{ }^{-N}$ | 111' $15^{\prime \prime}$ | 106' 19.91" |
| 4 | Nautical |  | 04:19 AM | 04:39:39 | 07:49 PM | 20:09:16 | $66^{\prime} 58.43$ | $4^{\prime} 3.06{ }^{\text {² }}$ | 248' $49.75{ }^{\prime \prime}$ | 243' 54.66* |
|  |  |  |  |  |  |  | 293' 1.57 | $4^{\prime \prime} 18.06{ }^{\prime \prime} \mathrm{N}$ | 121' 16.93" | 116' $21.84^{\prime \prime}$ |
| 5 | Astro |  | 03:37 AM | 03:56:54 | 08:32 PM | 20:52:10 | $57^{\prime} 49.54$ | $4^{\prime} 2.34^{\prime \prime} \mathrm{N}$ | $238{ }^{\prime} 8.36^{\prime \prime}$ | 233' $13.27^{\prime \prime}$ |
|  |  |  |  |  |  |  | 30210.46 | $4^{\prime \prime} 18.72^{\prime \prime} \mathrm{N}$ | $132^{\prime \prime} 0.49^{\prime \prime}$ | 127' 5.4" |
| 6 | Moon |  | 11:57 AM | 12:16:52 | 04:57 AM | 05:17:00 | 69 ' 45.36 | $23^{\prime} 22.56{ }^{\circ} \mathrm{N}$ | 268' 5.84" | 263' 10.75* |
|  | Chebyshev | $\checkmark$ | 11:59 AM | 12:19:16 | 04:08 AM | 04:27:57 | $275{ }^{\prime} 0.34$ | $21^{\prime} 39.54{ }^{\prime \prime} \mathrm{N}$ | $82^{\prime} 27.85^{\prime \prime}$ | 77' $32.76^{\prime \prime}$ |
|  |  |  | 30-Mar-23 |  | 01-Apr-23 |  |  |  |  |  |



## 15 Great Circle

The application provides a separate sheet for calculating:

- Destination latitude and longitude given a bearing and distance (as below)
- Bearing and distance from start and destination latitude and longitude positions (next page)
Date
Time

Starting Latitude Starting Longitude
Destination Lattude Destination Longitude


| Destination Date <br> ETA Time <br> Time Taken | $\begin{array}{\|r\|} \hline \text { 1-Apr-23 } \\ \text { 1:56:32 } \\ 15.94 \mathrm{hrs} \\ \hline \end{array}$ |  |  |
| :---: | :---: | :---: | :---: |
| (1) Calculated Position |  |  |  |
| Destination Latitude | 34.9999 N | 34 N | 59.99" |
| Destination Longitude | 15.0016 W | 15 W | -0.10" |
| (2) Bearing/Distance |  |  |  |
| Bearing Distance | $\begin{gathered} \mathrm{n} / \mathrm{a} \\ \mathrm{n} / \mathrm{a} \\ \hline \end{gathered}$ |  |  |

Eearing
istance
-
(1) Calculated Position




The units are kilometres, statute miles or nautical miles. The model calculates the item left blank. Enter data to the cells in blue and leave blank the unknown item. The model will calculate either item and leave the known item blank.

| Inputs: |  |  |
| :---: | :---: | :---: |
| Date | 31-Mar-23 | Minutes |
| Time | 10:00:00 |  |
| Units | Nautical Miles |  |
|  | Degrees |  |
| Starting Latitude | 32 N | 0.00 |
| Starting Longitude | 14 W | -30.00 |
| Destination Latitude | 35 N | 0.00 |
| Destination Longitude | 15 W | 0.00 |
| Bearing | 000.00 T |  |
| Distance | - | nm |
| Speed | 11.40 kn |  |

Position:

| Destination Date | 1-Apr-23 |
| :--- | ---: |
| ETA Time | 1:56:30 |
| Time Taken | 15.94 hrs |

(1) Calculated Position

| Destination Latitude | n/a - |
| :--- | :--- |
| Destination Longitude | n/a - |


| (2) Bearing / Distance |  |
| :--- | ---: |
| Bearing | 352.22 T |
| Distance | 181.74 nm |

## 16 Background Data

### 16.1 Description

There are three schedules which contain data used by other schedules. These are:

- Aries - Background data for corrections, Stars look-up and Moon calculations.
- Positions - Schedule of SHA, Altitude and Bearing at the DR position, time and date.
- Data - Lookup table of polynomial data for the DR date.

This is an extract from the Aries schedule showing the annual coefficients:

| Year | P | Q | R |
| :---: | :---: | :---: | :---: |
| 1988 | -3.8470 | 77.2633 | 99.8897 |
| 1989 | -3.1157 | 77.2461 | 99.6382 |
| 1990 | -3.3702 | 77.2289 | 99.4008 |
| 1991 | -3.6251 | 77.2118 | 99.1631 |
| 1992 | -3.8804 | 77.1946 | 98.9250 |
| 1993 | -3.1507 | 77.1774 | 99.6719 |
| 1994 | -3.4071 | 77.1603 | 99.4326 |
| 1995 | -3.6640 | 77.1431 | 99.1929 |
| 1996 | -3.9212 | 77.1260 | 98.9529 |
| 1997 | -3.1930 | 77.1087 | 99.6982 |
| 1998 | -3.4505 | 77.0916 | 99.4579 |
| 1999 | -3.7078 | 77.0744 | 99.2177 |
| 2000 | -3.9523 | 77.0605 | 98.9817 |
| 2001 | -3.2217 | 77.0411 | 99.7300 |
| 2002 | -3.4828 | 77.0236 | 99.4887 |
| 2003 | -3.7354 | 77.0092 | 99.2517 |
| 2004 | -3.9908 | 76.9909 | 99.0146 |
| 2005 | -3.2630 | 76.9706 | 99.7608 |
| 2006 | -3.5156 | 76.9577 | 99.5237 |
| 2007 | -3.7738 | 76.9424 | 99.2783 |
| 2008 | -4.0293 | 76.9231 | 99.0413 |
| 2009 | -3.3014 | 76.9041 | 99.7871 |
| 2010 | -3.5568 | 76.8858 | 99.5504 |
| 2011 | -3.8062 | 76.8689 | 99.3020 |
| 2012 | -4.0772 | 76.8519 | 99.0900 |
| 2013 | -3.3342 | 76.8350 | 99.8190 |
| 2014 | -3.5890 | 76.8180 | 99.5810 |
| 2015 | -3.8445 | 76.8011 | 99.3400 |
| 2016 | -4.1181 | 76.7841 | 99.1054 |
| 2017 | -3.3675 | 76.7672 | 99.8380 |
| 2018 | -3.6248 | 76.7502 | 99.6030 |
| 2019 | -3.8828 | 76.7333 | 99.3620 |
| 2020 | -4.1591 | 76.7163 | 99.1600 |
| 2021 | -3.4063 | 76.6995 | 99.8831 |
| 2022 | -3.6615 | 76.6826 | 99.5387 |
| 2023 | -3.9178 | 76.6658 | 99.2978 |
| 2024 | -4.1954 | 76.6489 | 99.1127 |
| 2025 | -3.4425 | 76.6320 | 99.7759 |

[^12]Annual and Basic Decimal Data

| Item | Sight 1 | Sight 2 | Sight 3 |  |
| :--- | ---: | ---: | ---: | ---: |
| $\mathrm{N}:$ Year | 2023 |  |  |  |
| P: Sun Ephemeris | -3.9178 |  |  |  |
| Q: Sun Ephemeris | 76.6658 |  |  |  |
| R: Aries Correction | 99.2978 |  |  |  |
| PRadians | 0.017453293 |  |  |  |
| >Degrees | 57.29577951 |  |  |  |
| Days From 01/01/80 | 15796.38 dys | 15796.13 dys | 15796.19 dys | 15796.37 dys |
| Days from 01/01/2023 | 90.38 dys | 90.13 dys | 90.19 dys | 90.37 dys |
| Days from 01/3/2023 | 31.38 dys | 31.13 dys | 31.19 dys | 31.37 dys |
| Original Latitude | 50.5857 N | 50.5857 N | 50.5857 N | 50.5857 N |
| Original Longitude | 4.9182 W | 4.9182 W | 4.9182 W | 4.9182 W |
| Decimal Latitude | 50.5857 N | 50.5857 N | 50.5857 N | 50.5857 N |
| Decimal Longitude | 4.9182 W | 4.9182 W | 4.9182 W | 4.9182 W |
| Note: No iteration |  |  |  |  |
| Original Latitude-Decimal | 0.0000 N | 0.0000 N | 0.0000 N | 0.0000 N |
| Miles | 0.000 mls |  |  |  |
| Original Longitude-Decimal | 0.0000 E | 0.0000 E | 0.0000 E | 0.0000 E |
| Miles | 0.000 mls |  |  |  |
|  |  |  |  |  |

This displays the Zone or Local Mean Time to GMT conversion table and the calculation of sight times:
Lookup Table for Zone Time / GMT

| 0 | $7.50^{\prime}$ | $22.50^{\prime}$ | $37.50^{\prime}$ | $52.50^{\prime}$ | $67.50^{\prime}$ | $82.50^{\prime}$ | $97.50^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |

Transferred DR Positions

|  | DR Position |  |  | Sight (1) |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
|  | Time | Date | Serial | Time | Date | Serial |
| Longitude | -4.918 |  |  | -4.918 |  |  |
| Zone | $9: 00: 00$ | $31 / 3 / 23$ | 45016.375 | $3: 00: 00$ | $31 / 3 / 23$ | 45016.125 |
| Adjustment | 0.00 hrs | 0.000 | 0.000 | 0.00 hrs | 0.000 | 0.000 |
|  | 0.375 | $31 / 3 / 23$ | 45016.375 | 0.125 | $31 / 3 / 23$ | 45016.125 |
| GMT | $9: 00: 00$ | $31 / 3 / 23$ | 45016.375 | $3: 00: 00$ | $31 / 3 / 23$ | 45016.125 |

This is the Positions schedule on 31 March 2023 at GMT 9:0:0 from the DR position $50^{\prime} \mathrm{N} 35.14$ " $5^{\prime} \mathrm{W} 55.09^{\prime \prime}$.

| Date: | 09:00:00 GMT | 31-Mar-23 | Select: | DR :9:0 ZT $: 50^{\prime} 35.14^{\prime \prime} \mathrm{N} \mathrm{4'} 55.09^{\prime \prime} \mathrm{W}$ |  |
| :--- | :---: | :--- | :--- | :--- | :--- |
| Aries: | $323.3756^{\prime}$ | $322.5518^{\prime}$ |  |  |  |
| L: | 808.6005 dys |  |  |  |  |


| No | Star Name | DR Days | GHA | GHA | Aries/SHA | LHA | LHA | DEC | DEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Sun | 11.9289' | 313.9329' | 313' 55.98' | 313.9329' | $309.0148^{\prime \prime}$ | 309' $0.89{ }^{\prime \prime}$ | 4.1132 N | $4^{\prime} 6.79{ }^{-N}$ |
| 1 | Venus | $9.5968^{\prime \prime}$ | 278.9522 | $278{ }^{\prime \prime} 57.13^{\prime \prime}$ | 278.9522' | 274.0340' | $274{ }^{\prime} 2.04{ }^{\prime \prime}$ | 17.8744 N | $17^{\prime} 52.46^{\prime \prime} \mathrm{N}$ |
| 2 | Mars | $6.3522^{\prime}$ | 230.2824 | $230^{\prime} 16.94{ }^{\prime \prime}$ | $230.2824^{\prime}$ | $225.3642^{\prime \prime}$ | 225' $21.85{ }^{\prime \prime}$ | 25.4812 N | 25' $28.87^{\prime \prime N}$ |
| 3 | Jupiter | 11.3712 | 305.5674' | 305' $34.04{ }^{\prime \prime}$ | 305.5674' | 300.6492 | 300' $38.95{ }^{\prime \prime}$ | 6.4394 N | $6^{\prime} 26.37^{\prime \prime} \mathrm{N}$ |
| 4 | Saturn | 14.2247' | $348.3700^{\prime}$ | $348^{\prime \prime} 22.2{ }^{\prime \prime}$ | $348.3700^{\prime}$ | $343.4518^{\prime}$ | 343' $27.11^{\prime \prime}$ | 11.7661 S | 11'45.97"S |
| 1 | Moon | $323.3756^{\prime}$ | $197.5916^{\prime}$ | $197^{\prime} 35.49^{\prime \prime}$ | $197.5916^{\prime}$ | 192.6734 ${ }^{\prime}$ | $192^{\prime} 40.4{ }^{\prime \prime}$ | 24.7411 N | $24^{\prime} 44.46{ }^{\prime \prime} \mathrm{N}$ |
| 1 | 1 Alpheratz | 1041.0920 ${ }^{\prime}$ | 321.0920 ${ }^{\prime}$ | 321' $5.52^{\prime \prime}$ | 357.7164' | $316.1738^{\prime \prime}$ | 316'10.43" | 29.2155 N | 29'12.93"N |
| 2 | 2 Ankaa | 1036.6318' | 316.6318' | $316^{\prime} 37.91^{\prime \prime}$ | $353.2562^{\prime}$ | $311.7136^{\prime \prime}$ | 311' $42.82^{\prime \prime}$ | 42.1820 S | $42^{\prime \prime} 10.92^{\prime \prime} \mathrm{S}$ |
| 3 | 3 Schedar | 1033.0357' | 313.0357' | $313^{\prime} 214^{\prime \prime}$ | $349.6600^{\prime \prime}$ | 308.1175' | 308' $7.05{ }^{\prime \prime}$ | 56.6628 N | 56'39.77"N |
| 4 | 4 Diphda | 10322997 | 8183997 | 1121798 | 348 92240 | 307.3815 ${ }^{\prime}$ | 307' $22.89{ }^{\prime \prime}$ | 17.8622 S | 17' 51.73"S |
| 5 | 5 Achernar | 1018.8457 | 298.8457' | 298' $50.74^{\prime \prime}$ | $335.470{ }^{\prime}$ | 293.9275' | 293' 55.65" | 57.1217 S | $57^{\prime} 7.3^{\prime \prime} \mathrm{S}$ |
| 6 | 6 Hamal | 1011.3673' | 291.3673' | 291' $22.04{ }^{\prime \prime}$ | $327.9917^{\prime}$ | $286.4492^{\prime}$ | 286' $26.95{ }^{\prime \prime}$ | 23.5702 N | $23^{\prime} 34.21{ }^{\circ} \mathrm{N}$ |
| 7 | 7 Acamar | 998.7020' | 278.7020 | $278^{\prime \prime} 42.12^{\prime \prime}$ | $315.3263^{\prime}$ | 273.7838' | 273' 47.03" | 40.2155 S | 40'12.93"S |
| 8 | 8 Menkar | $997.6137^{\prime}$ | 277.6137 | $277^{\prime} 36.82^{\prime \prime}$ | $314.2380^{\prime}$ | $272.6955^{\prime}$ | 272' 41.73' | 4.1782 N | $4^{\prime \prime} 10.69{ }^{\prime \prime} \mathrm{N}$ |
| 9 | 9 Mirfak | $991.9932^{\prime \prime}$ | 271.9932 | 271' $59.59^{\prime \prime}$ | $308.6176{ }^{\prime}$ | 267.0750' | $267^{\prime} 4.5^{\prime \prime}$ | 49.9440 N | $49^{\prime} 56.64{ }^{\prime \prime} \mathrm{N}$ |
| 10 | 10 Aldebaran | 974.1726' | 254.1726 ${ }^{\prime}$ | $254{ }^{\prime} 10.35^{\prime \prime}$ | 290.7969' | $249.2544^{\prime}$ | 249' $15.26{ }^{\prime \prime}$ | 16.5546 N | $16^{\prime} 33.28^{\prime \prime} \mathrm{N}$ |
| 11 | 11 Rigel | $964.5713^{\prime}$ | 244.5713 | $244^{\prime} 34.28^{\prime \prime}$ | 281.1957' | 239.6531' | 239'39.19' | 8.1778 S | 8' $10.67{ }^{\prime \prime} \mathrm{S}$ |
| 12 | 12 Capella | $963.8848^{\prime \prime}$ | 243.8848' | 243' $53.09^{\prime \prime}$ | 280.5092' | $238.9666^{\prime}$ | 238' $58^{\prime \prime}$ | 46.0227 N | $46^{\prime} 1.36{ }^{\prime \prime} \mathrm{N}$ |
| 13 | 13 Bellatrix | $961.8905^{\prime}$ | 241.8905 | $2411^{\prime} 53.43^{\prime \prime}$ | 278.5149' | 236.9723' | 236' 58.34" | 6.3688 N | $6^{\prime} 22.13^{\prime \prime} \mathrm{N}$ |
| 14 | 14 Elnath | 961.5452' | 241.5452' | 241'32.71" | $278.1695^{\prime}$ | $236.6270^{\prime \prime}$ | 236' $37.62^{\prime \prime}$ | 28.6269 N | $28^{\prime} 37.61^{\circ} \mathrm{N}$ |
| 15 | 15 Alnilam | $959.1364{ }^{\prime}$ | 239.1364' | 239' $8.18^{\prime \prime}$ | $275.7608^{\prime \prime}$ | $234.2182^{\prime \prime}$ | 234' 13.09' | 1.1895 S | 1'11.37"S |
| 16 | 16 Betelgeuse | 954.3769' | 234.3769' | 234' $22.61{ }^{\prime \prime}$ | 271.0013' | $229.4587^{\prime}$ | 229' $27.52^{\prime \prime}$ | 7.4097 N | $7{ }^{\prime} 24.58{ }^{\prime \prime} \mathrm{N}$ |
| 17 | 17 Canopus | $947.3660^{\prime \prime}$ | 227.3660 | 227' $21.96{ }^{\prime \prime}$ | 263.9904' | 222.4479' | 222' $26.87^{\prime \prime}$ | 52.7128 S | $52^{\prime \prime} 42.77^{\prime \prime} \mathrm{S}$ |
| 18 | 18 Sirius | 1301.9401' | 221.9401 ${ }^{\prime}$ | 221' 56.41" | 258.5645' | 217.0219' | $217^{\prime} 1.32^{\prime \prime}$ | 16.7513 S | $16^{\prime \prime} 45.08^{\prime \prime} \mathrm{S}$ |
| 19 | 19 Adhara | 1298.5978' | 218.5978' | $218^{\prime} 35.87^{\prime \prime}$ | $255.2221^{\prime}$ | $213.6796^{\prime}$ | 213' $40.78^{\prime \prime}$ | 29.0076 S | $29^{\prime} 0.45{ }^{\prime \prime} \mathrm{S}$ |
| 20 | 20 Procyon | 1288.3529' | 208.3529' | 208' $21.18^{\prime \prime}$ | 244.9773' | $203.4348^{\prime \prime}$ | 203' $26.09^{\prime \prime}$ | 5.1638 N | $5^{\prime} 9.83{ }^{\prime \prime} \mathrm{N}$ |
| 21 | 21 Pollux | 1286.7981' | 206.7981' | $206{ }^{\prime} 47.89{ }^{\prime \prime}$ | $243.4225^{\prime}$ | 201.8800' | 201' $52.8{ }^{\prime \prime}$ | 27.9706 N | $27^{\prime} 58.24^{\prime \prime} \mathrm{N}$ |
| 22 | 22 Avior | 1277.7324' | 197.7324' | $197{ }^{\prime} 43.94{ }^{\prime \prime}$ | 234.3567 | 192.8142' | $192^{\prime \prime} 48.85{ }^{\prime \prime}$ | 59.5880 S | $59^{\prime} 35.28^{\prime \prime} \mathrm{S}$ |
| 23 | 23 Suhail | 1266.2667' | $186.2667^{\prime}$ | $186^{\prime} 16^{\prime \prime}$ | 222.8911' | 181.3485' | 181' $20.91{ }^{\prime \prime}$ | 43.5298 S | 43' $31.79^{\prime \prime} \mathrm{S}$ |
| 24 | 24 Miaplacidus | 1265.1147 | 185.1147' | $185{ }^{\prime} 6.88^{\prime \prime}$ | 221.7390 ${ }^{\prime}$ | 180.1965 ${ }^{\prime}$ | 180' 11.79' | 69.8159 S | $69^{\prime} 48.95^{\prime \prime} \mathrm{S}$ |
| 25 | 25 Alphard | 1261.2977' | 181.2977' | 181' 17.86" | $217.9220^{\prime \prime}$ | 176.3795' | 176' $22.77^{\prime \prime}$ | 8.7613 S | $8^{\prime \prime} 45.68{ }^{\prime \prime} \mathrm{S}$ |
| 26 | 26 Regulus | 1251.0772 | 171.0772 | $1711^{\prime} 4.63^{\prime \prime}$ | $207.7016^{\prime}$ | 166.1591' | $166^{\prime} 9.54{ }^{\prime \prime}$ | 11.8529 N | $11^{\prime} 51.18^{\prime \prime} \mathrm{N}$ |
| 27 | 27 Dubhe | 1237.1851' | 157.1851' | 157' 11.11" | 193.8095' | $152.2670^{\prime}$ | $152^{\prime \prime} 16.02^{\prime \prime}$ | 61.6272 N | 61' 37.63 "N |
| 28 | 28 Denebola | 1225.9169' | 145.9169' | 145' 55.01" | 182.5413' | 140.9987 | $140^{\prime} 59.92^{\prime \prime}$ | 14.4412 N | $14^{\prime} 26.47^{\prime \prime} \mathrm{N}$ |
| 29 | 29 Gienah | 1219.2275' | 139.2275 ${ }^{\prime}$ | 139' 13.65" | $175.8518^{\prime}$ | 134.3093' | 134' 18.56" | 17.6723 S | $17^{\prime \prime} 40.34^{\prime \prime} \mathrm{S}$ |
| 30 | 30 Acrux | 1216.4977' | 136.4977' | $136^{\prime} 29.86^{\prime \prime}$ | 173.1221' | $131.5796^{\prime \prime}$ | 131' $34.77^{\prime \prime}$ | 63.2282 S | $63^{\prime \prime} 13.69{ }^{\prime \prime} \mathrm{S}$ |
| 31 | 31 Gacrux | 1215.3594' | 135.3594' | $135{ }^{\prime} 21.56^{\prime \prime}$ | 171.9838' | 130.4412' | 130' $26.47^{\prime \prime}$ | 57.2437 S | $57^{\prime} 14.62^{\prime \prime} \mathrm{S}$ |
| 32 | 32 Alioth | 1209.7101' | 129.7101' | 129 ' 42.61" | $166.3345^{\prime}$ | 124.7920 ${ }^{\prime \prime}$ | $124^{\prime} 47.52^{\prime \prime}$ | 55.8329 N | $55^{\prime} 49.97^{-N}$ |
| 33 | 33 Spica | 1201.8735' | 121.8735 ${ }^{\prime}$ | 121' $52.41^{\prime \prime}$ | 158.4979' | 116.9554' | 116' 57.32" | 11.2837 S | 11'17.02"S |
| 34 | 34 Alkaid | 1196.3600' | $116.3600^{\prime}$ | $116^{\prime} 21.6^{\prime \prime}$ | 152.9843' | 111.4418' | 111' $26.51{ }^{\prime \prime}$ | 49.1953 N | $49^{\prime \prime} 11.72^{\prime \prime} \mathrm{N}$ |
| 35 | 35 Hadar | 1192.1060' | 112.1060 | $112^{\prime} 6.36^{\prime \prime}$ | $148.7304^{\prime}$ | 107.1879' | 107' 11.27" | 60.4834 S | 60' $29.01{ }^{\prime \prime} \mathrm{S}$ |
| 36 | 36 Menkent | 1191.4644' | 111.4644' | $111{ }^{\prime} 27.86^{\prime \prime}$ | $148.0888^{\prime}$ | 106.5462 | 106' $32.77^{\prime \prime}$ | 36.4840 S | $36^{\prime} 29.04{ }^{\prime \prime} \mathrm{S}$ |
| 37 | 37 Arcturus | $1189.2973^{\prime}$ | 109.2973' | 109' 17.84" | 145.9217' | 104.3792 | 104' $22.75{ }^{\prime \prime}$ | 19.0592 N | $19{ }^{\prime} 3.55{ }^{\prime \prime} \mathrm{N}$ |
| 38 | 38 Rigul Kentaurus | 1183.1770' | 103.1770 | 103' $10.62^{\prime \prime}$ | $139.8014^{\prime \prime}$ | $98.2588^{\prime \prime}$ | $98^{\prime \prime} 15.53{ }^{\prime \prime}$ | 60.9287 S | 60' $55.72^{\prime \prime} \mathrm{S}$ |
| 39 | 39 Zubenelgenubi | 1180.4376 ${ }^{\prime}$ | 100.4376 ${ }^{\prime}$ | $100^{\prime} 26.25{ }^{\prime \prime}$ | 137.0619' | 95.5194' | $95^{\prime} 31.16^{\prime \prime}$ | 16.1389 S | $16^{\prime} 8.33$ "S |
| 40 | 40 Kochab | 1180.7955 ${ }^{\circ}$ | 100.7955 | $100^{\prime} 47.73^{\prime \prime}$ | $137.4198^{\prime \prime}$ | $95.8773^{\prime}$ | $95^{\prime} 52.64{ }^{-1}$ | 74.0566 N | $74^{\prime} 3.4^{4} \mathrm{~N}$ |
| 41 | 41 Alphecca | 1169.5603' | 89.5603' | $89^{\prime} 33.62^{\prime \prime}$ | 126.1847' | 84.6421' | $84^{\prime} 38.53{ }^{\prime \prime}$ | 26.6331 N | 26' $37.99^{\prime \prime} \mathrm{N}$ |
| 42 | 42 Antares | 1155.7721' | $75.7721^{\prime}$ | $75^{\prime} 46.33^{\prime \prime}$ | $112.3965^{\prime}$ | $70.8539^{\prime}$ | $70^{\prime} 51.24{ }^{\prime \prime}$ | 26.4829 S | $26^{\prime} 28.97^{\prime \prime} \mathrm{S}$ |
| 43 | 43 Atria | 1150.6943' | $70.6943{ }^{\prime}$ | $70^{\prime} 41.66^{\prime \prime}$ | $107.3186^{\prime}$ | $65.7761^{\prime}$ | $65^{\prime} 46.57{ }^{\prime \prime}$ | 69.0648 S | $69^{\prime} 3.89$ 'S |
| 44 | 44 Sabik | 1145.5537' | $65.5537{ }^{\prime}$ | $65^{\prime} 33.22^{\prime \prime}$ | 102.1781' | $60.6355^{\prime}$ | $60^{\prime} 38.13^{\prime \prime}$ | 15.7540 S | $15^{\prime} 45.24{ }^{\prime \prime} \mathrm{S}$ |
| 45 | 45 Shaula | 1139.6855' | 59.6855' | $59^{\prime} 41.13^{\prime \prime}$ | $96.3098{ }^{\prime \prime}$ | $54.7673^{\prime}$ | $54^{\prime} 46.04{ }^{\prime \prime}$ | 37.1188 S | $37^{\prime} 7.13{ }^{\prime \prime} \mathrm{S}$ |
| 46 | 46 Rasalhague | $1139.4783^{\prime}$ | 59.4783' | $59^{\prime} 28.7^{\prime \prime}$ | 96.1027 | 54.5602' | $54^{\prime} 33.61{ }^{\prime \prime}$ | 12.5398 N | $12^{\prime \prime} 32.39^{\prime \prime} \mathrm{N}$ |
| 47 | 47 Eltanin | 1134.1942' | 54.1942' | $54^{\prime \prime} 11.65^{\prime \prime}$ | $90.8185{ }^{\prime}$ | $49.2760^{\prime}$ | $49^{\prime} 16.56{ }^{\prime \prime}$ | 51.4798 N | 51' $28.79{ }^{\prime \prime} \mathrm{N}$ |
| 48 | 48 Kaus Australis | 1127.0553' | 47.0553' | 47'3.32' | 83.6796' | 42.1371 ${ }^{\prime \prime}$ | $42^{\prime} 8.23^{\prime \prime}$ | 34.3721 S | $34^{\prime} 22.33^{\prime \prime} \mathrm{S}$ |
| 49 | 49 Vega | 1124.0514' | 44.0514' | $44^{\prime} 3.09{ }^{\prime \prime}$ | 80.6758' | 39.1333' | $39^{\prime \prime} 8^{\prime \prime}$ | 38.7996 N | $38^{\prime \prime} 47.98^{\prime \prime} \mathrm{N}$ |

## 17 Data Schedules

### 17.1 Description

There are several schedules used to calculate the GHA and DEC. These are for:

| Sun | $1=$ Sun |
| :--- | :--- |
| Star | $2=$ Star |
| Moon | $3=$ Moon |
| Planet | $4=$ Venus, $5=$ Mars, $6=$ Jupiter, $7=$ Saturn |

This data is for the period 1991-2025. If the model is used outside these dates, it will prompt you for Almanac or revised polynomial data. This is an extract from the Stars schedule:

| No | Identification |  |  | Constellation | Abreviation |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Star | Mag | Letter |  |  |
| 1 | Alpheratz | 2.2 | A | Andromedae | And |
| 2 | Ankaa | 2.4 | A | Phoenicis | Phe |
| 3 | Schedar | 2.5 | A | Cassiopaiae | Cas |
| 4 | Diphda | 2.2 | B | Ceti | Cet |
| 5 | Achernar | 0.6 | A | Eridani | Eri |
| 6 | Hamal | 2.2 | A | Arietis | Ari |
| 7 | Acamar | 3.1 | H | Eridani | Eri |
| 8 | Menkar | 2.8 | A | Ceti | Cet |
| 9 | Mirfak | 1.9 | A | Persei | Per |
| 10 | Aldebaran | 1.1 | A | Tauri | Tau |
| 11 | Rigel | 0.3 | B | Orionis | Ori |
| 12 | Capella | 0.2 | A | Aurigae | Aur |
| 13 | Bellatrix | 1.7 | C | Orionis | Ori |
| 14 | Elnath | 1.8 | A | Tauri | Tau |
| 15 | Alnilam | 1.8 | E | Orionis | Ori |
| 16 | Betelgeuse | 0.5 | A | Orionis | Ori |
| 17 | Canopus | -0.9 | A | Carinae | Car |
| 18 | Sirius | -1.6 | A | Canis Majoris | CMa |
| 19 | Adhara | 1.6 | E | Canis Majoris | CMa |
| 20 | Procyon | 0.5 | A | Canis Minoris | CMi |
| 21 | Pollux | 1.2 | B | Geminorum | Gem |
| 22 | Avior | 1.7 | E | Carinae | Car |
| 23 | Suhail | 2.2 | L | Velorum | Vel |
| 24 | Miaplacidus | 1.8 | B | Carinae | Car |
| 25 | Alphard | 2.2 | A | Hydrae | Hya |
| 26 | Regulus | 1.3 | A | Leonis | Leo |
| 27 | Dubhe | 2.0 | A | Ursae Majoris | UMa |
| 28 | Denebola | 2.2 | B | Leonis | Leo |
| 29 | Gienah | 2.8 | C | Corvi | Cry |
| 30 | Acrux | 1.1 | A | Crucis | Cru |
| 31 | Gacrux | 1.6 | C | Crucis | Cru |
| 32 | Alioth | 1.7 | E | Ursae Majoris | UMa |
| 33 | Spica | 1.2 | A | Virginis | Vir |
| 34 | Alkaid | 1.9 | G | Ursae Majoris | UMa |
| 35 | Hadar | 0.9 | B | Centauri | Cen |
| 36 | Menkent | 2.3 | H | Centauri | Cen |
| 37 | Arcturus | 0.2 | A | Bootis | Boo |
| 38 | Rigul Kentaurus | 0.1 | A | Centauri | Cen |
| 39 | Zubenelgenubi | 2.9 | A | Librae | A2Lib |
| 40 | Kochab | 2.2 | B | Ursae Minoris | UMi |

## 18 Worked Examples

### 18.1 Sun, Moon and a Star on 21 June 1994

Check the Scenarios in the application (2003: Tools Scenarios, 2007+: Data, What-if, Scenarios) as all the examples are included in the model.

A ship at ZT 22:0:0 (GMT 23:0:0) on 21 June 1994 calculated its DR Position as $32^{\prime} 0^{\prime \prime} \mathrm{N} 15^{\prime} 0^{\prime \prime} \mathrm{W}$ and has followed a course of $325.00^{\prime} \mathrm{T}$ at a speed of 8 knots per hour for several hours. Three sights have been taken and a fix is now sought to check the transferred positions.

The individual sights are :
(1) Sun at ZT 18:0:0 (GMT 19:0:0) at an altitude of 11' 57.0"
(2) Moon at ZT 18:23:30 at an altitude of 11' $34.0^{\prime \prime}$
(3) Star thought to be Kochab (40) at ZT 21:23:20 at an altitude of 46' $31.0^{\prime \prime}$ and a bearing of 356' $0.0^{\prime \prime}$.

At $15^{\prime} \mathrm{W}$ the model calculates the local time as:

$$
\text { GMT }+15^{\prime} \mathrm{W} /(360 / 24)=\text { GMT }-1 \text { hour (the usual convention for West and South is negative). }
$$

The star finder and identification routines are used to ensure the accurate selection of the star. A following page shows the location of all Navigational Stars for the DR time and position in this example. Summary of results:

|  | Sun | Moon | Star (Kochab 40) |
| :---: | :---: | :---: | :---: |
| Time of Sight (GMT) | 19:00:00 | 19:23:00 | 22:23:20 |
| Difference to DR Time | (4 h 00 m ) | ( 3 h 36 m ) | (0 h 36 m ) |
| Observed Angle | $11^{\prime} 57.0{ }^{\prime \prime}$ | $11^{\prime} 34.0{ }^{\prime \prime}$ | 47'31.0" |
| Adjusted Altitude | 12' $8.35{ }^{\prime \prime}$ | 12'44.94" | 47'30.09" |
| Declination | 23' $26.29{ }^{\prime \prime} \mathrm{N}$ | 20' 17.28" S | 74' $10.93{ }^{\prime \prime} \mathrm{N}$ |
| GHA | 104' $33.7{ }^{\prime \prime}$ | 314' $48.56{ }^{\prime \prime}$ | 23' $1.61{ }^{\prime \prime}$ |
| LHA | 89' 53" | 300' 5.79" | 8' 2.59 " |
| Azimuth /Bearing | 290' 14.09" | 123' 42.94" | 356' 45.86" |
| Intercept / Distance | 3.60 Miles | 3.51 Miles | 3.26 Miles |
| Direction | Towards | Towards | Away |

The Model uses the 'Method of Least Squares' to compute a fix at the DR Time of 31'N 55.78' 15 'W 2.88'. This position is on a bearing of 211.07 ' T 4.87 miles from the DR Position.

The results also show the confidence ellipse using standard deviation at $95 \%$ with its angle bearing 42.48 ' T. The length of the ellipse is 6.88 miles and its width 13.03 miles.

| DR Position: |  |  |  | Calculated Position: |  | Position Error: |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DR Latitude |  | $32 . \mathrm{N}$ | $0.00{ }^{\prime \prime}$ | $31^{\prime} \mathrm{N}$ | 55.78" | Confidence |  |
| DR Longitude | v | $15^{\prime} \mathrm{W}$ | $0.00^{\prime \prime}$ | $15^{\prime} \mathrm{W}$ | 2.88" | Ellipse | 95.00\% |
| DR Zone Date |  | 21-Jun-94 | Tuesday |  |  |  |  |
| Zone / GMT |  | 22:00:00 | 23:00 GMT | Distance | Bearing | Latitude | 6.88 mls |
| Course / Speed |  | 325.00 T | 8.00 kn | 4.87 mls | 211.07 T | Longitude | 13.03 mls |
| Temperature \& Pressure |  | $9.80{ }^{\circ} \mathrm{C}$ | 1010.00 mb |  |  | Bearing | 042.48 T |
| Sight \# 1 |  |  |  | Sight \# 2 |  | Sight \# 3 |  |
| Which Sight | 1 Sun |  |  | 3 Moon |  | 2 Star |  |
| Calc/Almanac/Polynomial | B Polynomial |  |  | B Polynomial |  | B Polynomial |  |
| Star Number | 49 |  |  | 0 |  | 40 Kochab |  |
| Actual Sight Time |  | 18:00:00 | 19:00 GMT | 18:23:00 | 19:23 GMT | 21:23:20 | 22:23 GMT |
| Time Diff. / Miles |  | 4:00 hrs | 32.00 mls | 3:37 hrs | 28.93 mls | 0:36 hrs | 4.89 mls |
| Revised DR Position |  | $31^{\prime} 33.8^{\prime \prime} \mathrm{N}$ | $14^{\prime} 38.4{ }^{\text {" }} \mathrm{W}$ | $31^{\prime} 36.3^{\prime \prime} \mathrm{N}$ | $14^{\prime} 40.4{ }^{\prime \prime} \mathrm{W}$ | $31^{\prime} 56^{\prime \prime} \mathrm{N}$ | $14^{\prime} 56.7^{\prime \prime} \mathrm{W}$ |
| DR Alt. / Bearing |  | 12 ' $4.74{ }^{\prime \prime}$ | 290 '14.29 ${ }^{\prime \prime}$ | 12 ' 41.1" | 123 ' $46.47^{\prime \prime}$ | 47 ' 33.34 | 356 ' $44.69^{\prime \prime}$ |
| Observed Angle |  | $11^{\prime} 57^{\prime \prime}$ |  | $11^{\prime \prime} 34^{\prime \prime}$ |  | $47^{\prime \prime} 31^{\prime \prime}$ |  |
| Index Error: Minutes |  | 0.00' |  | $0.00{ }^{\prime \prime}$ |  | 0.00' |  |
| Height of User's Eye / DIP |  | $0.00^{\prime \prime}$ |  | $0.00{ }^{\prime \prime}$ |  | 0.00' |  |
| Refraction ( $\mathrm{R}=\mathrm{Ro}^{*} \mathrm{f}$ ) |  | $4.56{ }^{\prime \prime}$ |  | $4.60{ }^{\prime \prime}$ |  | 0.91" |  |
| Parallax in Altitude |  | 0.14" |  | $59.00^{\prime \prime}$ |  | 0.00' |  |
| Semi-Diameter |  | 15.76" |  | 16.41" |  | 0.00" |  |
| Corrected Altitude |  | $12^{\prime \prime} 8.35^{\prime \prime}$ |  | $12^{\prime} 44.6^{\prime \prime}$ |  | $47^{\prime \prime} 30.09^{\prime \prime}$ |  |
| Calc. Declination |  | $23^{\prime} 26.29^{\prime \prime}$ | North | -20' 17.64" | South | $74^{\prime} 10.93^{\prime \prime}$ | North |
| Sun GHA / LHA |  | $104{ }^{\prime} 33.7^{\prime \prime}$ | 89' 55.34" | 314' 50.11" | $300^{\prime} 9.68{ }^{\prime \prime}$ | $23^{\prime} 1.61^{\prime \prime}$ | 8'4.91" |
| Azimuth / Bearing |  | 290' $14.29^{\prime \prime}$ | 290' 14.29' | 123' $46.47^{\prime \prime}$ | 123' $46.47^{\prime \prime}$ | 356' $44.69^{\prime \prime}$ | 176' $44.69^{\prime \prime}$ |
| Intercept : Miles |  | 3.60 mls | Towards | 3.51 mls | Towards | 3.26 mls | Away |
| Calc. Position |  | $31^{\prime} 35{ }^{\prime \prime} \mathrm{N}$ | $14^{\prime} 42.2^{\prime \prime} \mathrm{W}$ | $31^{\prime} 34.4{ }^{\prime \prime} \mathrm{N}$ | $14^{\prime} 37.1^{\circ} \mathrm{W}$ | $31^{\prime} 52.9{ }^{\prime \prime} \mathrm{N}$ | $14^{\prime} 56.5^{\prime \prime} \mathrm{W}$ |



### 18.2 Regulus, Antares and Kochab on 4 July 1994

This example is taken from The Nautical Almanac 1994 (HMSO) ${ }^{17}$.
Required: calculate the position of a ship on 4 July 1994 at GMT 21:0:0 which has been travelling on a constant course of $325^{\prime} \mathrm{T}$ for several hours at a speed of 20 knots.

Three observations have been taken:

| Sight No | Number/Star | GMT / Universal Time | Adjusted Altitude |
| :---: | :---: | :---: | :---: |
| Sight (1) | (26) Regulus | GMT 20:39:23 | $27.0109^{\prime}$ |
| Sight (2) | (42) Antares | GMT 20:45:47 | $26.0764^{\prime}$ |
| Sight (3) | (40) Kochab | GMT 21:10:34 | $47.4449^{\prime}$ |

The time is GMT 21:0:0 and the estimated position (DR) is $32^{\prime} \mathrm{N} 15^{\prime} \mathrm{W}$.
No Hour Angle, Declination and corrections to the Observed Angle are needed with Systematic Navigation and the intermediate results using the same format as The Nautical Almanac 1994 (HMSO) are:

| Star: | Regulus | Antares | Kochab |
| :---: | :---: | :---: | :---: |
| Star Number: | 26 | 42 | 40 |
| Time of Observation | 20:39:23 UT | 20:45:47 UT | 21:10:34 UT |
| Adjusted Altitude ( $\mathrm{H}_{\mathrm{O}}$ ) | 27.0109' | 26.0764' | 47.4449' |
| Greenwich Hour Angle | 80.4516 ${ }^{\prime}$ | 346.7984' | $17.6023{ }^{\prime}$ |
| Local Hour Angle | 65.5084' | 331.8312' | $2.5424{ }^{\prime}$ |
| Time Difference to DR | -0.3436 hours | -0.2369 hours | +0.1761 hours |
| Revised Latitude | $31.5250{ }^{\prime} \mathrm{N}$ | $31.5730^{\prime} \mathrm{N}$ | $31.6480{ }^{\prime} \mathrm{N}$ |
| Revised Longitude | 14.9320 ' W | 14.9790 ' W | $15.0590^{\prime} \mathrm{W}$ |
| Azimuth (Z) | 267.7551' | $151.9161^{\prime}$ | 358.9752' |
| Calculated Altitude ( $\mathrm{H}_{\mathrm{c}}$ ) | $27.0210^{\prime}$ | $26.0983 '$ | 47.4647 |
| Distance (p) | +0.0100' | +0.0220' | +0.0198 ${ }^{\prime}$ |
| Intercept (I) | 0.60 miles | 1.32 miles | 1.19 miles |
| Direction | Away | Away | Away |

The Almanac calculates a final estimated position of $31.6193^{\prime} \mathrm{N} 15.0204^{\prime} \mathrm{W}\left(31^{\prime} \mathrm{N} 37.158^{\prime \prime} 15^{\prime} \mathrm{W} 1.224\right.$ " $)$.
The fix using the model is $31^{\prime} \mathrm{N} 37.13$ " $15^{\prime} \mathrm{W} 1.22^{\prime \prime}$ at a distance from the DR position of 22.90 miles on a bearing of 182.71' T .

The system print-out is on the next page.

[^13]| DR Position: |  |  | Calculated Position: | Position Error: |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| DR Latitude | $32^{\prime} \mathrm{N}$ | $0.00^{\prime \prime}$ | $31^{\prime} \mathrm{N}$ | $37.13^{\prime \prime}$ | Confidence | Ellipse |



### 18.3 Sun, Moon and Star on 19 June 1991

This example appears on page xxii of Compact Data 1991. On 19/6/91 at GMT 21:00 the DR position of a ship is $32^{\prime \prime} 45^{\prime \prime}$ $\mathrm{N} 15^{\prime} 30^{\prime \prime} \mathrm{W}$ and it has followed a course of $325^{\prime} \mathrm{T}$ at a constant speed of 12 knots for several hours.

| Sight | Time | Altitude | Height |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
| (1) Sun | 18:15:24 GMT | $21^{\prime} 25.398^{\prime \prime}$ | 6.0 metres |
| (2) Moon | 20:30:45 GMT | $46^{\prime} 32.700^{\prime \prime}$ | 6.0 metres |
| (3) Vega (49) | 20:42:23 GMT | $29^{\prime} 27.132^{\prime \prime}$ | 6.0 metres |

Using a further sight of Dubhe (27) the fix gained by Compact Data is $32^{\prime} 39.1^{\prime \prime} \mathrm{N} 15^{\prime} 34.2^{\prime \prime} \mathrm{W}$ and this compares well with the answer below, given that the Moon is calculated using Method 'A with Aries coefficients.

| DR Position: |  |  |  | Calculated Position: |  | Position Error: |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DR Latitude |  | 32 N | 45.00" | 32 ' N | 35.92" | Confidence |  |
| DR Longitude | , | 15 W | -30.00" | 15 ' W | $29.33^{\prime \prime}$ | Ellipse | 95.00\% |
| DR Zone Date |  | 19-Jun-91 | Wednesday |  |  |  |  |
| Zone / GMT |  | 20:00:00 | 21:00 GMT | Distance | Bearing | Latitude | 3.09 mls |
| Course / Speed |  | 325.00 T | 12.00 kn | 9.10 mls | 176.27 T | Longitude | 4.95 mls |
| Temperature \& Pressure |  | $9.80{ }^{\circ} \mathrm{C}$ | 1010.00 mb |  |  | Bearing | 331.42 T |
| Sight \# 1 |  |  |  | Sight \# 2 |  | Sight \# 3 |  |
| Which Sight Calc/Almanac/Polynomial | 1 Sun B Polynomial |  |  | $\begin{gathered} 3 \text { Moon } \\ \text { A Calculated } \end{gathered}$ |  | 2 Star B Polynomial |  |
| Star Number | 0 |  |  | 0 |  | 49 Vega |  |
| Actual Sight Time |  | 17:15:24 | 18:15 GMT | 19:30:45 | 20:30 GMT | 19:42:23 | 20:42 GMT |
| Time Diff. / Miles |  | 2:44 hrs | 32.92 mls | 0:29 hrs | 5.85 mls | 0:17 hrs | 3.52 mls |
| Revised DR Position |  | $32^{\prime \prime} 9 \mathrm{~m}$ | $15^{\prime} 6.9$ " W | $32^{\prime \prime} 31.1^{\prime \prime} \mathrm{N}$ | $15^{\prime} 25.3$ " W | $32^{\prime} 33^{\prime \prime} \mathrm{N}$ | $15^{\prime} 26.9{ }^{\text {m W }}$ |
| DR Alt. / Bearing |  | $21^{\prime} 33.65{ }^{\prime \prime}$ | 284 ${ }^{\prime} 51.89$ " | $47^{\prime} 25.2^{\prime \prime}$ | 204 '2.47" | 29 '24.01 | 60 ' $27.27^{\prime \prime}$ |
| Observed Angle |  | $21^{\prime} 25.4{ }^{\text {- }}$ |  | $46^{\prime} 32.7{ }^{\prime \prime}$ |  | 29' $27.13^{\prime \prime}$ |  |
| Index Error: Minutes |  | 0.00" |  | $0.00{ }^{\prime \prime}$ |  | 0.00" |  |
| Height of User's Eye / DIP |  | -4.31" |  | $0.00{ }^{\prime \prime}$ |  | $0.00{ }^{\prime \prime}$ |  |
| Refraction ( $\mathrm{R}=\mathrm{Ro}{ }^{*} \mathrm{f}$ ) |  | 2.53 " |  | 0.87" |  | $1.76{ }^{\prime \prime}$ |  |
| Parallax in Altitude |  | $0.13{ }^{\prime \prime}$ |  | $39.02^{\prime \prime}$ |  | 0.00" |  |
| Semi-Diameter |  | 15.77" |  | 15.46" |  | $0.00{ }^{\prime \prime}$ |  |
| Corrected Allitude |  | 21' $34.47^{\prime \prime}$ |  | $47^{\prime} 26.17^{\prime \prime}$ |  | $29^{\prime} 25.37^{\prime \prime}$ |  |
| Calc. Declination |  | 23' $25.53^{\prime \prime}$ | North | -7' 11.56" | South | 38' $46.45{ }^{\prime \prime}$ | North |
| Sun GHA / LHA |  | 93' $32.15^{\prime \prime}$ | $78^{\prime} 25.24^{\prime \prime}$ | 31' $33.21^{\prime \prime}$ | $16^{\prime} 7.87^{\prime \prime}$ | 298' $59.86^{\prime \prime}$ | 283' $32.94{ }^{\prime \prime}$ |
| Azimuth / Bearing |  | 284' 51.89" | 284' 51.89" | 204' $2.47^{\prime \prime}$ | 204' $2.47^{\prime \prime}$ | 60' $27.27^{\prime \prime}$ | 60' $27.27^{\prime \prime}$ |
| Intercept: Miles |  | 0.82 mls | Towards | 0.96 mls | Towards | 1.36 mls | Towards |
| Calc. Position |  | $32^{\prime} 9.2^{\circ} \mathrm{N}$ | $15^{\prime} 7.8^{\circ} \mathrm{W}$ | $32^{\prime} 30.3{ }^{\prime} \mathrm{N}$ | $15^{\prime} 25.8{ }^{\circ} \mathrm{W}$ | $32^{\prime} 33.7{ }^{\prime \prime N}$ | $15^{\prime} 25.6{ }^{\text {W }}$ W |

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### 18.4 Vega, Moon and Sun on 15 February 2006

This example applies the theory from the previous sections to bring together the calculation of GHA, LHA, Declination with sight reduction and statistical fixes. This example is taken from Compact Data.

On February 15,2006 at GMT 11:0:0 the DR position is assumed to be $32^{\prime} \mathrm{N} 45^{\prime \prime} 15^{\prime} \mathrm{W} 30^{\prime \prime}$. Three sights have been taken along a course of $315^{\prime} \mathrm{T}$ at a speed of 12 knots. The temperature is $9.8^{\prime} \mathrm{C}$ and the atmospheric pressure 1010 Mb . The height of the eye above the horizon is 6.0 metres. Sextant index error is assumed to $0{ }^{1118}$.

|  | Star (Vega 49) | Moon | Sun |
| :--- | :---: | :---: | :---: |
| Time of Sight (GMT) | $6: 28: 52$ | $6: 33: 52$ | $9: 53: 45$ |
| Difference to DR Time | $(5.32 \mathrm{~h})$ | $(5.26 \mathrm{~h})$ | $(2.06 \mathrm{~h})$ |
| Observed Angle (Hs) | $48^{\prime} 5.2^{\prime \prime}$ | $28^{\prime} 26^{\prime \prime}$ | $23^{\prime} 58.9^{\prime \prime}$ |
| Adjusted Altitude (Ho) | $4^{\prime} 60^{\prime \prime}$ | $29^{\prime} 26.33^{\prime \prime}$ | $24^{\prime} 8.68^{\prime \prime}$ |
|  |  |  |  |
| Declination | $38^{\prime} 46.99^{\prime \prime} \mathrm{N}$ | $5^{\prime} 43.04^{\prime} \mathrm{N}$ | $12^{\prime} 39.53^{\prime \prime} \mathrm{S}$ |
| GHA | $323^{\prime} 3.758^{\prime \prime}$ | $73 '_{\prime \prime} 17.12^{\prime \prime}$ | $324^{\prime} 54.23^{\prime \prime}$ |
| LHA | $308^{\prime} 30.9^{\prime \prime}$ | $56^{\prime} 41.5^{\prime \prime}$ | $308^{\prime} 45.01^{\prime \prime}$ |
|  |  |  |  |
| Azimuth / Bearing | $65^{\prime} 45.64^{\prime \prime}$ | $257^{\prime} 27.11^{\prime \prime}$ | $126^{\prime} 42.51^{\prime \prime}$ |
| Intercept / Distance | 0.34 Miles | 0.39 Miles | 0.09 Miles |
| Direction | Towards | Towards | Towards |

The calculated position after several iterations is $32^{\prime} \mathrm{N} 44.06{ }^{\prime \prime}, 15^{\prime} \mathrm{W} 30.45$ ' a distance 1.02 miles and a bearing of 202.71 degrees from the DR position.


[^14]| DR Position: |  |  | Calculated Position: | Position Error: |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| DR Latitude | $32^{\prime} \mathrm{N}$ | $45.00^{\prime \prime}$ | $32^{\prime} \mathrm{N}$ | $44.06^{\prime \prime}$ | Confidence | Ellipse |



This is a listing of the visible planets and stars at the DR position at 6:30:0 GMT based on a minimum of 20' and a maximum of $80^{\prime}$. This sheet can be used to ascertain the potential bodies and show the approximate altitude and bearing.

| No | No | Star Name | Mag | C. Altitude | Bearing |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | Sun N/A |  | (15.63') | 95.25' |
| 2 |  | Venus N/A |  | $13.88^{\prime \prime}$ | $119.82^{\prime}$ |
| 3 |  | Mars N/A |  | (35.10') | 350.98' |
| 4 |  | Jupiter |  | $41.08{ }^{\prime \prime}$ | 182.32' |
| 5 |  | Saturn N/A |  | $3.07{ }^{\prime}$ | 291.11' |
| 6 |  | Moon |  | $29.9{ }^{\prime \prime}$ | 256.47' |
| 1 | 37 | 37 Arcturus | 0.2 | $71.44{ }^{\prime}$ | $226.34^{\prime}$ |
| 2 | 34 | 34 Alkaid | 1.9 | $67.1{ }^{\prime \prime}$ | 322.64' |
| 3 | 32 | 32 Alioth | 1.7 | $56.76{ }^{\prime}$ | 324.61' |
| 4 | 47 | 47 Eltanin | 2.4 | 54.89' | $45.36{ }^{\prime}$ |
| 5 | 46 | 46 Rasalhague | 2.1 | $51.65{ }^{\prime}$ | $113.36^{\prime}$ |
| 6 | 49 | 49 Vega | 0.1 | 48.57' | $66.63{ }^{\prime}$ |
| 7 | 40 | 40 Kochab | 2.2 | 48.54' | 357.77' |
| 8 | 27 | 27 Dubhe | 2 | 41.54' | $326.00^{\prime}$ |
| 9 | 39 | 39 Zubenelgenu | 2.9 | 40.92' | $186.74{ }^{\prime}$ |
| 10 | 28 | 28 Denebola | 2.2 | 40.61' | 260.89' |
| 11 | 33 | 33 Spica | 1.2 | 39.19' | $214.68^{\prime}$ |
| 12 | 44 | 44 Sabik | 2.6 | $33.87{ }^{\prime}$ | 145.09' |
| 13 | 58 | 58 Polaris | 2.1 | $33.44{ }^{\prime}$ | 0.13' |
| 14 | 42 | 42 Antares | 1.2 | 28.01' | 160.37' |
| 15 | 53 | 53 Deneb | 1.3 | $27.63{ }^{\prime}$ | 51.89' |
| 16 | 29 | 29 Gienah | 2.8 | $24.38^{\prime \prime}$ | 226.71' |
| 17 | 51 | 51 Altair | 0.9 | 21.85' | 93.45' |
| 18 | N/A | N/A | N/A | N/A | 256.47' |
| 19 | N/A | N/A | N/A | N/A | 256.47' |
| 20 | N/A | N/A | N/A | N/A | 256.47' |



### 18.5 Moon, Star (18 Sirius) and Mars on 11 September 2014

On September 11, 2014 at GMT 06:30:0 the DR position is assumed to be $32^{\prime} \mathrm{N} 1$ " $15^{\prime} \mathrm{W} 38^{\prime \prime}$. Three sights have been taken along a course of $315^{\prime} \mathrm{T}$ at a speed of 12 knots. The temperature is $9.8^{\prime} \mathrm{C}$ and the atmospheric pressure 1010 Mb . The height of the eye above the horizon is 6.0 metres. Sextant index error is assumed to $0,{ }^{״ 19}$.

|  | Moon | Star | Mars |
| :---: | :---: | :---: | :---: |
| Time of Sight (GMT) | 5:54:52 | 6:05:21 | 6:15:235 |
| Difference to DR Time | (0.35 h) | (0.24 h) | (0.14 h) |
| Observed Angle (Hs) | $30^{\prime} 26.6{ }^{\prime \prime}$ | 32'42.9" | 47' 10.4" |
| Adjusted Altitude (Ho) | 31' $21.82^{\prime \prime}$ | 32' 37.04" | 47'5.22" |
| Declination | 8' $46.45{ }^{\prime \prime} \mathrm{N}$ | $1643.82{ }^{\text {S }}$ | $21^{\prime} 36.81{ }^{\prime \prime} \mathrm{N}$ |
| GHA | 72' 52.1" | 342 ' $47.9{ }^{\prime \prime}$ | 327' $28.1{ }^{\prime \prime}$ |
| LHA | 58' 19.94" | 328 14.01" | 312' $52.54{ }^{\prime \prime}$ |
| Azimuth / Bearing | 260' 13.21" | 143' 15.08" | 91' 54.05" |
| Intercept / Distance | 2.17 Miles | 2.42 Miles | 3.73 Miles |
| Direction | Away | Towards | Towards |

The calculated position after several iterations is 32 ' $\mathrm{N} 0.02^{\prime \prime}, 14^{\prime} \mathrm{W} 34.46$ " a distance 3.154 miles and a bearing of 107.38 degrees from the DR position.

| DR Position: |  |  |  | Calculated Position: |  | Position Error: |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DR Latitude |  | $32 . \mathrm{N}$ | 1.00" | $32^{\prime} \mathrm{N}$ | 0.02" | Confidence |  |
| DR Longitude | v | $14^{\prime} \mathrm{W}$ | -38.00" | 14 ' W | $34.46^{\prime \prime}$ | Ellipse | 95.00\% |
| DR Zone Date |  | 14-Sep-11 | Wednesday |  |  |  |  |
| Zone / GMT |  | 5:30:00 | 06:30 GMT | Distance | Bearing | Latitude | 1.50 mls |
| Course/ Speed |  | 315.00 T | 12.00 kn | 3.15 mls | 107.38 T | Longitude | 2.99 mls |
| Temperature \& Pressure |  | $9.80{ }^{\circ} \mathrm{C}$ | 1010.00 mb |  |  | Bearing | 011.31 T |
|  | Sight \# 1 |  |  | Sight \# 2 |  | Sight \# 3 |  |
| Which Sight | 3 Moon <br> B Polynomial |  |  | 2 Star |  | 5 Mars |  |
| Calc/Almanac/Polynomial |  |  |  | B Polynomial |  |
| Star Number |  | 49 |  |  |  | 18 Sirius |  | 0 |  |
| Actual Sight Time |  | 4:54:57 | 05:54 GMT | 5:05:21 | 06:05 GMT | 5:15:23 | 06:15 GMT |
| Time Diff. / Miles |  | 0:35 hrs | 7.01 mls | 0:24 hrs | 4.93 mls | 0:14 hrs | 2.92 mls |
| Revised DR Position |  | $31^{\prime} 56^{\prime \prime} \mathrm{N}$ | $14^{\prime} 32.2^{\text {m }} \mathrm{W}$ | $31^{\prime \prime} 57.5^{\prime \prime} \mathrm{N}$ | $14^{\prime} 33.9^{\prime \prime} \mathrm{W}$ | $31^{\prime} 58.9^{\prime \prime} \mathrm{N}$ | $14^{\prime} 35.6^{\prime \prime} \mathrm{W}$ |
| DR Alt. / Bearing |  | $31^{\prime} 24^{\prime \prime}$ | 260 ' 13.21" | 32 ' $34.62^{\prime \prime}$ | $143{ }^{\prime \prime} 15.08^{\prime \prime}$ | 47'1.49 | 91 '54.05" |
| Observed Angle |  | $30^{\prime} 26.598^{\prime \prime}$ |  | $32^{\prime \prime} 42.9{ }^{\prime \prime}$ |  | 47' 10.4 " |  |
| Index Error: Minutes |  | $0.00{ }^{\prime \prime}$ |  | $0.00{ }^{\prime \prime}$ |  | 0.00' |  |
| Height of User's Eye / DIP |  | -4.31" |  | -4.31" |  | -4.31" |  |
| Refraction ( $\mathrm{R}=\mathrm{Ro} 0^{\star} \mathrm{f}$ ) |  | 1.61" |  | 1.55" |  | 0.93" |  |
| Parallax in Altitude |  | $46.60^{\prime \prime}$ |  | $0.00^{\prime \prime}$ |  | 0.05" |  |
| Semi-Diameter |  | 14.71" |  | 0.00" |  | $0.00{ }^{\prime \prime}$ |  |
| Corrected Altitude |  | 31' $21.82^{\prime \prime}$ |  | $32^{\prime \prime} 37.04^{\prime \prime}$ |  | $47^{\prime} 5.22^{\prime \prime}$ |  |
| Calc. Declination |  | $8^{\prime \prime} 46.45^{\prime \prime}$ | North | $-16^{\prime} 43.82^{\prime \prime}$ | South | $21^{\prime} 36.81{ }^{\prime \prime}$ | North |
| Moon GHA / LHA |  | 72' 52.1" | 58'19.94" | $342^{\prime \prime} 47.9^{\prime \prime}$ | 328' 14.01" | 327' $28.1^{\prime \prime}$ | 312' 52.54" |
| Azimuth / Bearing |  | 260' 13.21" | 80' 13.21" | 143' 15.08" | 143' 15.08" | 91' $54.05^{\prime \prime}$ | 91' 54.05" |
| Intercept : Miles |  | 2.17 mls | Away | 2.42 mls | Towards | 3.73 mls | Towards |
| Calc. Position |  | $31^{\prime} 56.4{ }^{\prime \prime} \mathrm{N}$ | $14^{\prime} 29.7^{*} \mathrm{~W}$ | $31^{\prime} 55.7^{\prime \prime} \mathrm{N}$ | $14^{\prime} 32.3{ }^{\circ} \mathrm{W}$ | $31^{\prime} 58.8{ }^{\prime \prime} \mathrm{N}$ | $14^{\prime} 31.3{ }^{\prime \prime} \mathrm{W}$ |

[^15]


### 18.6 Moon, Star (37 Acturus) and Mars on 2 April 2016

On April 2, 2016 at GMT 12:00:0 the DR position is assumed to be $33^{\prime} \mathrm{N} 24^{\prime \prime} 15^{\prime} \mathrm{W} 42^{\prime \prime}$. Three sights have been taken along a course of $315^{\prime} \mathrm{T}$ at a speed of 12 knots. The temperature is $9.8^{\prime} \mathrm{C}$ and the atmospheric pressure 1010 Mb . The height of the eye above the horizon is 6.0 metres. Sextant index error is assumed to $0{ }^{020}$.

|  | Moon | Star | Mars |
| :---: | :---: | :---: | :---: |
| Time of Sight (GMT) | 6:04:27 | 6:14:17 | 5:19:43 |
| Difference to DR Time | (5.55 h) | (5:45 h) | (5.4 h) |
| Observed Angle (Hs) | 29'30.4" | 38' $42.1{ }^{\prime \prime}$ | $31^{\prime} 28.8{ }^{\prime \prime}$ |
| Adjusted Altitude (Ho) | 30' 30.19" | $38^{\prime} 36.55{ }^{\prime \prime}$ | 31' 22.03 " |
| Declination | 15' $43.01{ }^{\prime \prime} \mathrm{S}$ | $195.86{ }^{\prime} \mathrm{N}$ | 20'43.71" S |
| GHA | 338' 18.83 " | 70' 29.54 " | 40' 2.08" |
| LHA | 323' $39.17^{\prime \prime}$ | 55' 48.22" | $25^{\prime} 19.83$ '" |
| Azimuth / Bearing | 138' $32.77^{\prime \prime}$ | 269' 12.84" | 207' 57.43" |
| Intercept / Distance | 1.27 Miles | 1.36 Miles | 1.10 Miles |
| Direction | Towards | Towards | Away |

The calculated position after several iterations using the switch on the right of the Inputs sheet is 33 ' N 26.08 ", 15 ' W 39.91 " a distance 2.713 miles and a bearing of 41.12 degrees from the DR position.

|  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |

[^16] $15.6593^{\prime} \mathrm{W}\left(15^{\prime} \mathrm{W} 39.6^{\prime \prime}\right) . \mathrm{a}=5.089 \mathrm{~nm}, \mathrm{~b}=3.959 \mathrm{~nm}$, azimuth $\theta=19^{\prime}$ using the same methods for four rather than three observations.



### 18.7 Moon, Star (34 Alkaid) and Sun on 1 May 2021

On May 1, 2021 at GMT 12:00:0 the DR position is assumed to be $32^{\prime} \mathrm{N} 45^{\prime \prime} 15^{\prime} \mathrm{W} 30^{\prime \prime}$. Three sights have been taken along a course of $315^{\prime} \mathrm{T}$ at a speed of 12 knots. The temperature is $10^{\prime} \mathrm{C}$ and the atmospheric pressure 1010 Mb . The height of the eye above the horizon is 6.0 metres. Sextant index error is assumed to $0{ }^{י 21}$.

|  | Moon | Star | Mars |
| :---: | :---: | :---: | :---: |
| Time of Sight (GMT) | 5:21:57 | 5:35:24 | 9:53:45 |
| Difference to DR Time | (6.38 h) | (6:24 h) | (2.06 h) |
| Observed Angle (Hs) | 31' 16.9" | 28' $46.8^{\prime \prime}$ | 44' $46.4{ }^{\prime \prime}$ |
| Adjusted Altitude (Ho) | 32' 18.08" | 28' 40.72 " | 44' 57.08 " |
| Declination | 25' 33.9" S | $4912.51{ }^{\prime} \mathrm{N}$ | $15^{\prime} 12.17{ }^{\prime \prime} \mathrm{S}$ |
| GHA | 21' 9.29" | $96^{\prime} 7.26^{\prime \prime}$ | 329'10.08" |
| LHA | 6' 46.22" | 81' 41.93 " | $314^{\prime} 1.31^{\prime \prime}$ |
| Azimuth / Bearing | 187' 13.48" | $312{ }^{\prime} 32.9{ }^{\prime \prime}$ | 101' 17.57" |
| Intercept / Distance | 2.46 Miles | 1.29 Miles | 0.48 Miles |
| Direction | Towards | Towards | Away |

The calculated position after several iterations using the switch on the right of the Inputs sheet is 33 ' N 26.08 ", 15 ' W 39.91 " a distance 2.713 miles and a bearing of 41.12 degrees from the DR position.


[^17]


## 19 Information

### 19.1 Read Me Notes

## Systematic Navigation - Version 7.0 1-Jan-2021 : 'Registered' Copy

## CONTENTS

## Introduction

Explanation of Systematic Navigation
Installation
Starting the Application - Systematic Navigation
Trial Copy Licence Agreement
Unless registered, this is an 'Evaluation' version which is valid for a 21 day evaluation period for a single position. The software is not free and after 21 days, you should register it and keep your conscience clear!

## Introduction

Systematic Navigation comprises a complete application in Microsoft Excel for astro navigation without tables or an almanac. It has been full revised and updated for the period 1991-2025 and should be of interest to navigators, astonomers and students particularly those studying for the yachtmaster examinations.

The model accepts up to three sextant sights taken from one position or along a course line. It then reduces the sights and derives an azimuth/bearing plot and an intercept in miles from the DR position. With two or more sights, Systematic Navigation will statistically calculate a fix position in latitude and longitude.

The results sheet summarises the results for each sight and draws a plot of the revised position.
The table below shows the extent of automatic calculation of the Greenwich Hour Angle and Declination. You can always use the model as a training aid and opt to enter all data and check your answers against the model.

Systematic Navigation uses both Method 'A' (Aries coefficents) or Method 'B' (Polynomial coefficients):

|  | Method A | Method B |
| :--- | :--- | :--- |
| Sun | Yes | $1991-2025$ |
| Stars | Enter Almanac Data | $1991-2025$ |
| Moon | Yes | $1991-2025$ |
| Planets | Enter Almanac Data | $1991-2025$ |

Systematic Navigation contains these separate schedules within the file:
(1) Input form for up to three sights of the sun, moon, stars and planets
(2) Results with a chart plot and fix
(3) Chart Plot and sun, moon and planetary positions
(4) Star charts at the DR time
(5) Positions schedule of the sun, moon, stars and planets
(6) Sun and moon rise and set
(7) Great Circle navigation
(8) Background calculations and aries coefficients
(9) Read Me and Registration

Please contact Alastair Day if you would like assistance or further information on this or any other of our products. We welcome suggestions and look forward to hearing from you.

Copyright (c) Systematic Finance Ltd. All rights reserved. All intellectual contents and any derivatives and improvements to this product, Systematic Navigation, are the property of Systematic Finance Ltd.

The program has been extensively tested. However no liability can be accepted regarding the use or accuracy of the programs whatsoever. We will make every effort to rectify any errors reported to us at the address below.

### 19.2 Installation

You need to install Systematic Navigation on a hard disk. Follow the instructions below:
The system requirements are an IBM compatible computer with minimum 3.0 Mb spare disk capacity. The software requirements are Windows and Excel 2003+..

The package contains all the files for this application.
(A) Unzip the files to a new directory C:ISFLNavXX
(B) The complete package contains the Excel file, pdf manual and ReadMe text
(C) Click the icon twice to start the application - Systematic Navigation.

### 19.3 Starting the Application

After installing Systematic Navigation, open it following the instructions below:
(A) Click the icon twice and the system will load Excel and Systematic Navigation.
(B) When you first open the system, it will display copyright information. Press to agree.
(C) The system opens Systematic Navigation.
(D) Press 'Halt' and tab to 'Version' to enter any licencing information.

Save this file with your results whenever you exit Systematic Navigation.
All reports were prepared with an HP 5 laser printer: if you have problems adjust the magnification in Print Preview. Keep all files in the same sub-directory - they will not work correctly if split between different directories.

### 19.4 Version and File Information

This is the Version sheet which is the last schedule on Systematic Navigation. The system displays this information at the bottom of each schedule.

A complete copy of Systematic Navigation is valid until 31 December 2025. After this date, the application will not work properly and will display error messages.

| Installation: | 1/1/2021 07:00:00 | Original installation date |
| :--- | :--- | :--- |
| Serial No: | 14197-121-7.0 | Licence serial number |
| Licence Type: | 'Registered' Copy | 'Shareware' or 'Registered' licence |
| Application: | Systematic Navigation | Initial macro screen |
| BoxName: | Systematic Navigation | Title of the macro dialog boxes |
| Version: | Version 7.0 1-Jan-2021 | Appears on all sheets to identify the version |
| Expiry Date: | 31 Dec 2025 | Data valid until 31-Dec-2025 |
| Price: | na | Normal price for Systematic Navigation |
| Contact: | (9 Systematic Navigation : www.sysmaps.co.uk | Copyright holder displayed on all schedules |
| Author: | Alastair Day | Author and copyright holder |
| Company: | Systematic Navigation | Company name and address |
| Address1: | Orchard House |  |
| Address2: | Green Lane |  |
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We would like to thank the authors of these publications which proved to be invaluable reference guides in the preparation of Systematic Navigation.

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## Alastair L Day

Guildford, 27 August 2020


[^0]:    ${ }^{1}$ See bibliography for Basic Astro Navigation by Conrad Dixon.

[^1]:    ${ }^{2}$ Explained in section 4.1.

[^2]:    ${ }^{3}$ Example from page 278 of The Nautical Almanac 1996. GHA $=149.7604^{\prime}, \mathrm{DEC}=11.3892^{\prime} \mathrm{S}$

[^3]:    ${ }^{4}$ Example from Macmillan \& Silk Cut Nautical Almanac Astro-Supplement 1996, Page 39. The answers given are DEC = N 16' 30 " and GHA $=324^{\prime} 34.8^{\prime \prime}\left(324.58^{\prime}\right)$. There is an addition error in the text since GHA(Aries) is calculated from the tables as $33.998^{\prime}$ and SHA as 291.0733'. These add up to 325.0716’ ( $325^{\prime} 4.2980^{\prime \prime}$ ) not 324.580’ ( $324^{\prime} 34.8^{\prime \prime}$ ).

[^4]:    ${ }^{5}$ Example from Macmillan \& Silk Cut Nautical Almanac Astro-Supplement 1997, Page 39. Answer given as 49'N 42 " for the latitude and 0 ' for the azimuth.

[^5]:    ${ }^{6}$ Example from pages 18 and 19 of Compact Data 1996.

[^6]:    ${ }^{7}$ See bibliography for Astro Navigation by Pocket Computer by Mike Harris. Algorithms are on page 69.
    ${ }^{8}$ Example from Compact Data 1996 Page 7. Answer given as GHA $=87.6592^{\prime}, \mathrm{DEC}=2.5688^{\prime}, \mathrm{HP}=0.996^{\prime}$

[^7]:    ${ }^{9}$ Example from the tables on page 68 of The Nautical Almanac 1996. GHA $=3.091667$ (3'5.5"), DEC $=0.4350{ }^{\prime}\left(0^{\prime} \mathrm{N} 26.1^{\prime \prime}\right)$

[^8]:    ${ }^{10}$ Example from page 19 of Compact Data 1996.

[^9]:    ${ }^{11}$ Example from page 281 of The Nautical Almanac 1996. Answers given are 21.4877 ', 34.4644 ' and 4.2935'. The slight differences on the Moon and Venus are explained by $0.005^{\prime}$ variation in the horizontal parallax. Their example also ignores the oblateness of the Earth which yields a small variation.
    ${ }^{12}$ Note that with a bubble sextant, no correction for height is needed.
    ${ }^{13}$ Formula from a paper by G G Bennett, 1982, Journal of the Institute of Navigation, volume 35, page 255 . The formula has now been revised to $\mathrm{Ro}=0.0167 / \tan (\mathrm{H}+7.32) /(\mathrm{h}+4.32))$
    ${ }^{14}$ Add lower limb and subtract upper limb.

[^10]:    ${ }^{15}$ Example from page 18 and 19 of Compact Data 1996 derives the same answers.

[^11]:    ${ }^{16}$ This is the complete worked example from pages 18 and 19 of Compact Data 1996. The answer given is $32.6554^{\prime} \mathrm{N}$ ( 32 ' $\mathrm{N} 39.3^{\prime \prime}$ ), $15.5387^{\prime} \mathrm{W}\left(15^{\prime} \mathrm{W} 32.3^{\prime \prime}\right)$. $\mathrm{a}=1.257 \mathrm{~nm}, \mathrm{~b}=2.485 \mathrm{~nm}$, azimuth $\theta=37^{\prime}$ using the same methods for four observations.

[^12]:    This extract shows the derivation of decimal time for each observation and the revised sight position:

[^13]:    ${ }^{17}$ Example from pages 282 and 283. Position calculated as $31.6193^{\prime}$ ( $31^{\prime} \mathrm{N}^{\prime} 37.158^{\prime \prime}$ ), $15.0204^{\prime} \mathrm{W}\left(15^{\prime} \mathrm{W} 1.224^{\prime \prime}\right)$

[^14]:    ${ }^{18}$ This is the complete worked example from pages 60 and 61 of Compact Data 2006. The answer given is $32.7211^{\prime} \mathrm{N}(32$ ' N 43.266 '), $15.4707^{\prime} \mathrm{W}\left(15^{\prime} \mathrm{W} 28.2420^{\prime \prime}\right)$. $\mathrm{a}=5.089 \mathrm{~nm}, \mathrm{~b}=3.959 \mathrm{~nm}$, azimuth $\theta=350^{\prime}$ using the same methods for four rather than three observations.

[^15]:    ${ }^{19}$ This adapted from the examplei from pages 18 and 19 of Compact Data 2010. The answer given for different times and positions is $32.788^{\prime} \mathrm{N}\left(32^{\prime} \mathrm{N} 47.3^{\prime \prime}\right), 15.508^{\prime} \mathrm{W}\left(15^{\prime} \mathrm{W} 30.5^{\prime \prime}\right) . \mathrm{a}=4.177 \mathrm{~nm}, \mathrm{~b}=1.816 \mathrm{~nm}$, azimuth $\theta=16^{\prime}$ using the same methods for four rather than three observations.

[^16]:    ${ }^{20}$ This is the complete worked example from pages 18 and 19 of Compact Data 2016-2020. The answer given is $33.4466^{\prime} \mathrm{N}$ ( $33^{\prime} \mathrm{N} 26.8^{\prime \prime}$ ),

[^17]:    ${ }^{21}$ This is the complete worked example from Compact Data 2011-2025. The answer given is $32.7309^{\prime} \mathrm{N}$ ( $32^{\prime} \mathrm{N} 43.9^{\prime \prime}$ ), $15.5365^{\prime} \mathrm{W}\left(15^{\prime} \mathrm{W}\right.$ $\left.32.2^{\prime \prime}\right) . \mathrm{a}=1.874 \mathrm{~nm}, \mathrm{~b}=3.335 \mathrm{~nm}$, azimuth $\theta=320$ ' using the same methods for four rather than three observations.

